
Part 3

Phase Diagrams and Alloys

Phase Diagrams

What are Phase diagrams?

Maps showing the equilibrium phase of a material at a given temperature and composition

Why study Phase diagrams?

Phase diagrams enable us to –

- select a phase

- select a processing route

- select a microstructure

Definitions - 1

- Component – Pure metal of which the alloy is composed
- Solute – Component of solid solution present in minor concentration
- Solvent – Component present in greatest amount
- Solubility limit – Maximum concentration of solute that can dissolve in solvent
- Phase – A homogenous portion of a system with uniform physical and chemical characteristics

Definitions -2

- Equilibrium – system whose thermodynamic free energy is a minimum
- Phase equilibrium – State achieved with minimum free energy in systems with more than one phase
- Metastable State – A state which has not reached equilibrium
- Equilibrium Phase Diagram – The relationship between the temperature and compositions of phases present at equilibrium

More Definitions

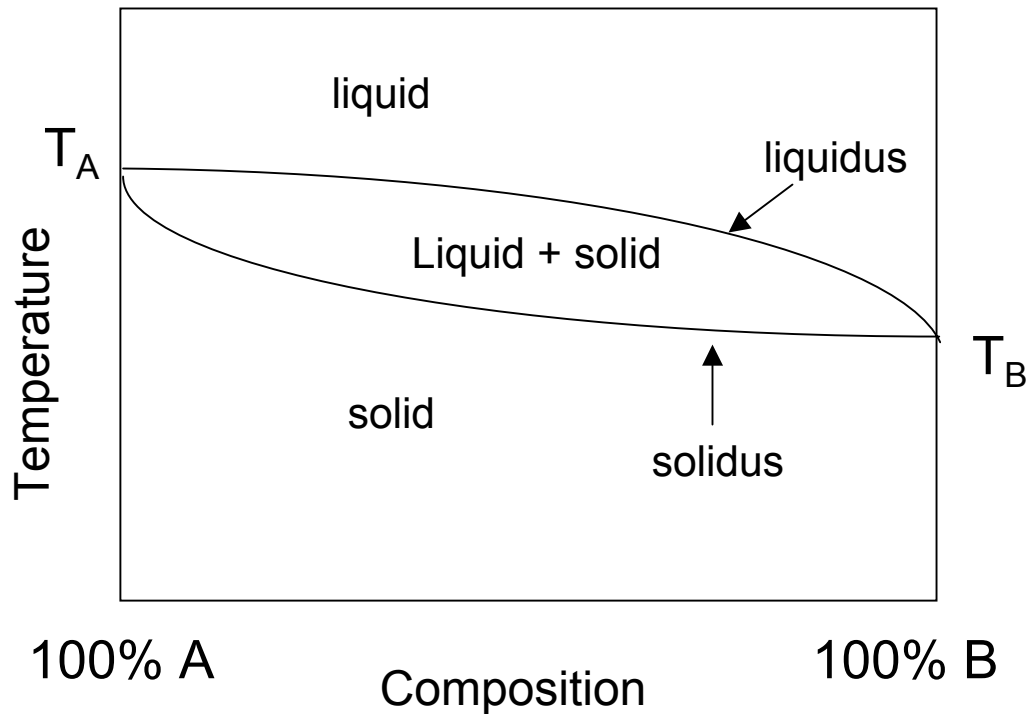
- Constitution
 - The constitution of an alloy is described by
 - the phases present
 - the weight fraction of each phase
 - the composition of each phase
- The equilibrium constitution is when the alloy has no further tendency to change at a given temperature and pressure

A simple binary phase diagram

Consider a mixture of 2 metals A and B

Solid exists as a solution at all temperature (isomorphous)

A solidifies at T_A : B solidifies at T_B



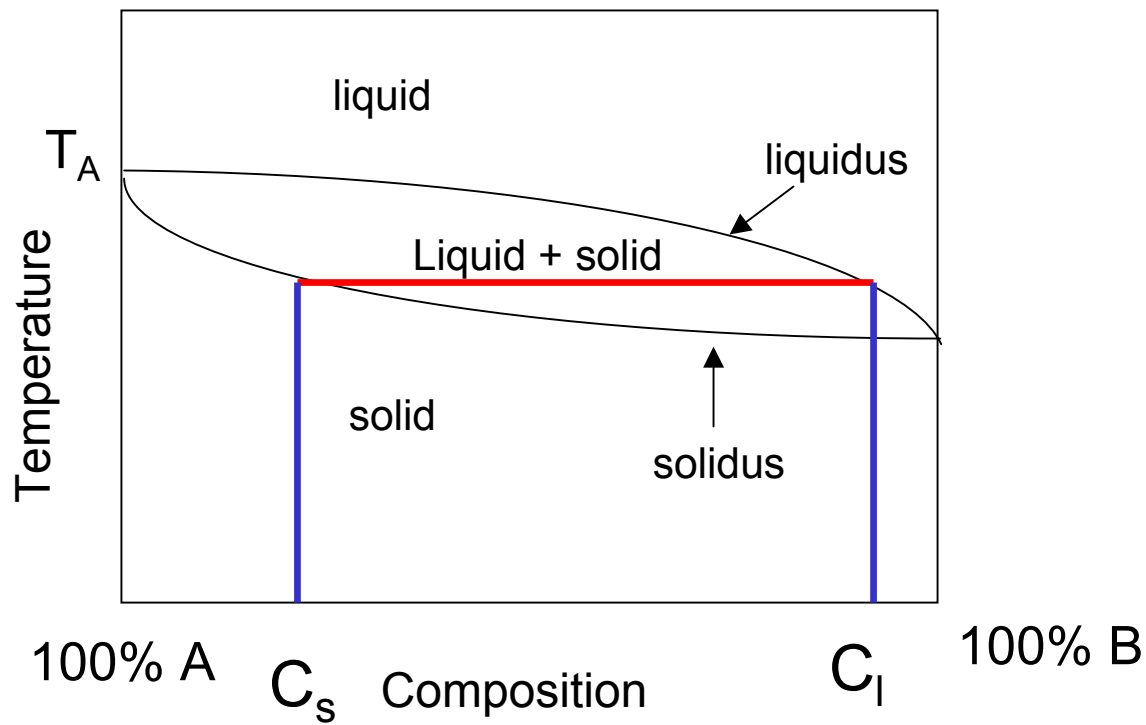
Liquidus – line at which solidification begins

Solidus – line at which solidification is completed

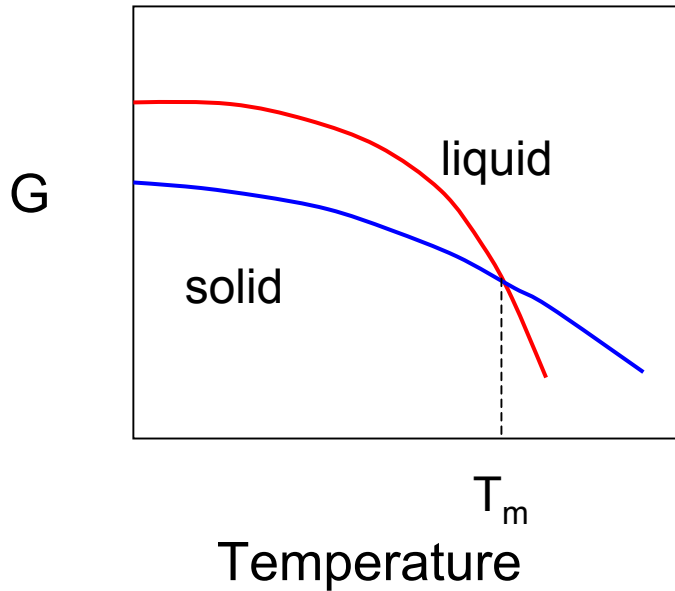
Tie Lines

Horizontal Isotherm at a given temperature

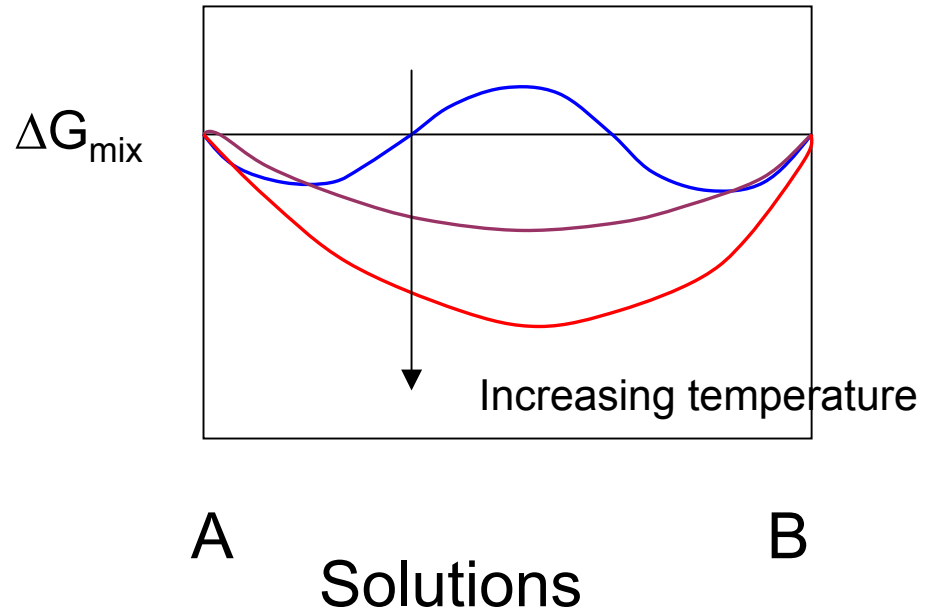
Determines compositions of the 2 phases
(liquid and solid)



Free energy considerations



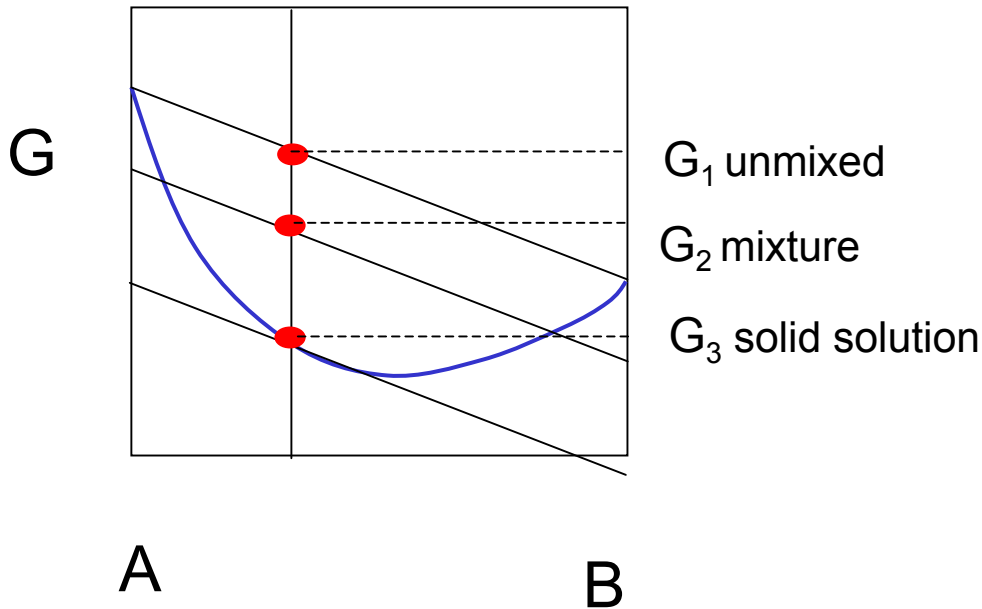
Pure substance



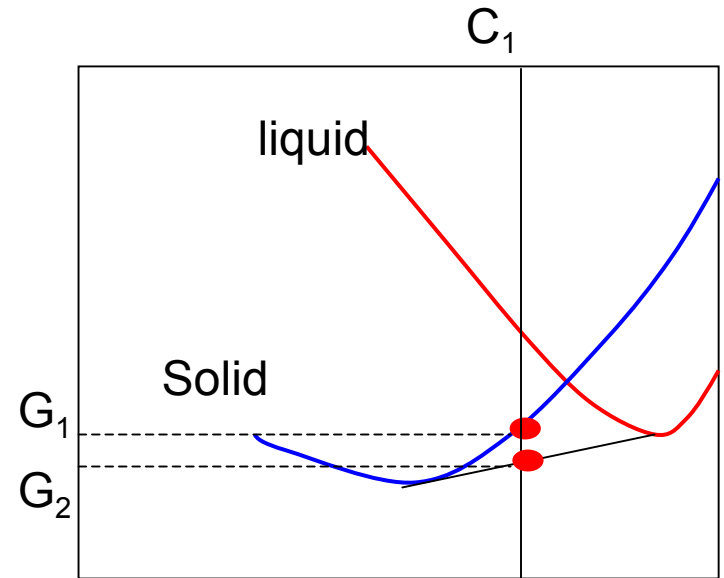
At high T there is complete solution and a single minimum in the free energy curve

$$\Delta G_{\text{mix}} = \Delta H_{\text{mix}} - T\Delta S_{\text{mix}} = x_A x_B \Omega + RT (x_A \ln x_A + x_B \ln x_B)$$

Free energy and phase diagrams



Single phase



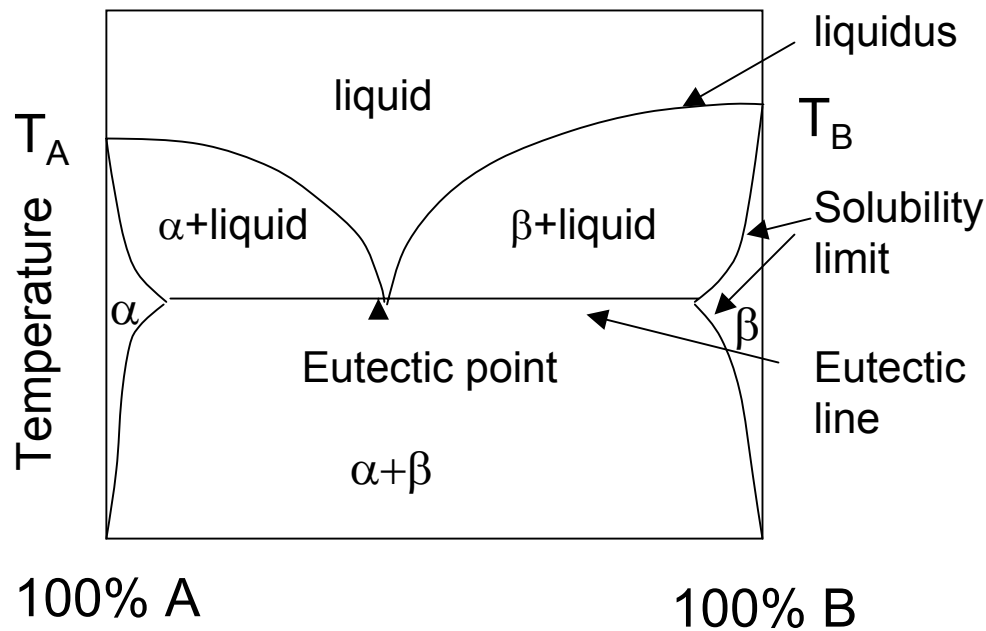
When more than 1 phase present system can reduce the free energy separating into 2 phases

When temperature is altered the compositions of solids and liquids in equilibrium change and build up the solidus and liquidus lines

A Binary Phase Diagram

Limited solubility of A in B and B in A
Consider a mixture of 2 metals A and B

A solidifies at T_A : B solidifies at T_B



Liquidus – line at which solidification begins

Eutectic line - solidification occurs

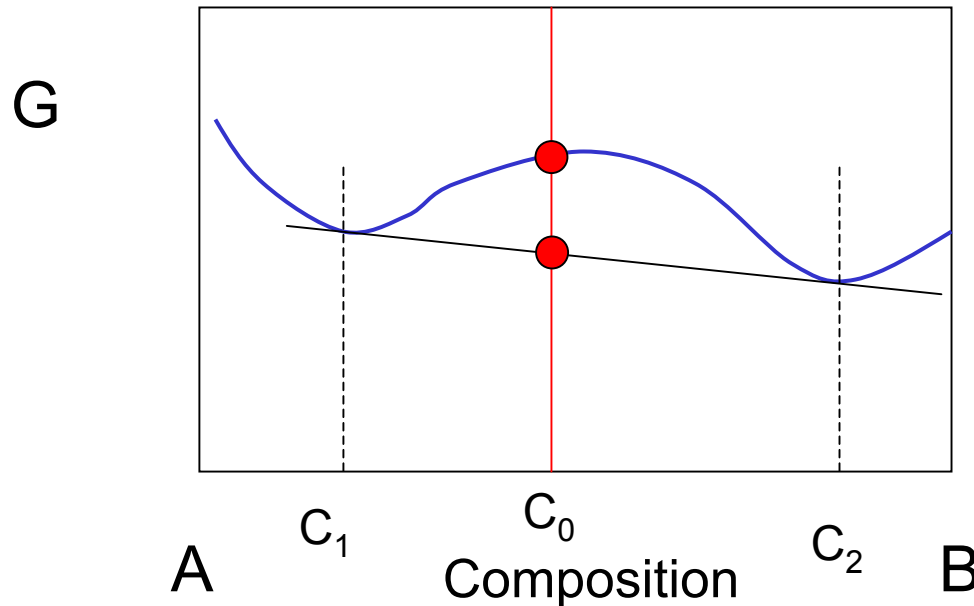
Eutectic point – lowest melting point

α – A rich solid solution

β – B rich solid solution

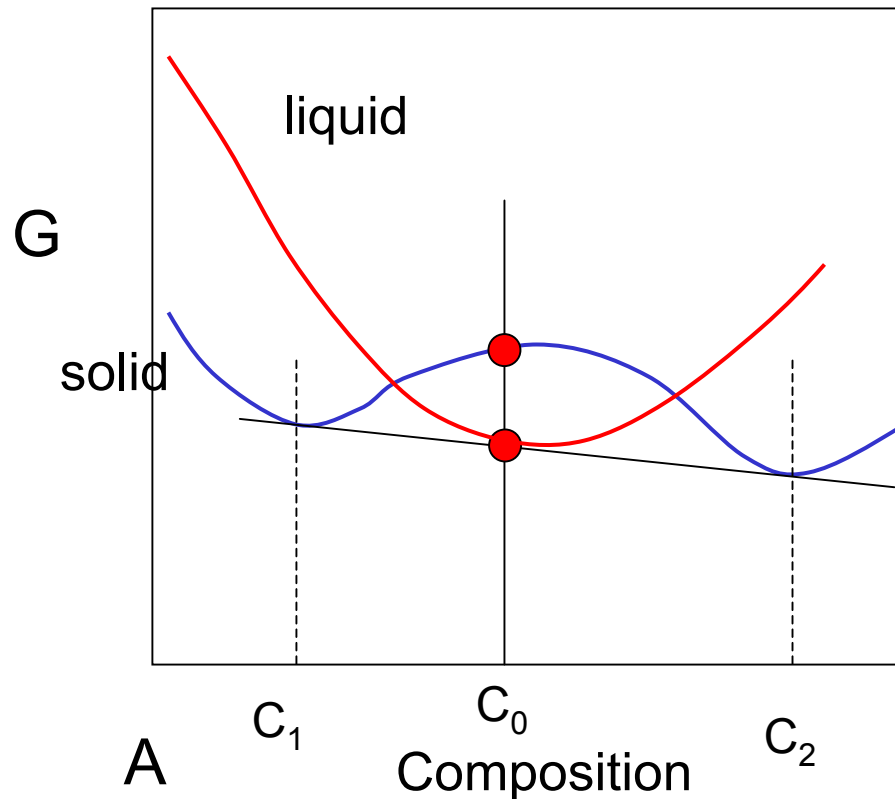
Free energy – binary phase diagrams

System can lower free energy by separating into 2 solid phases



Liquid may solidify as single phase but separates into 2 phases on further cooling

Eutectic systems

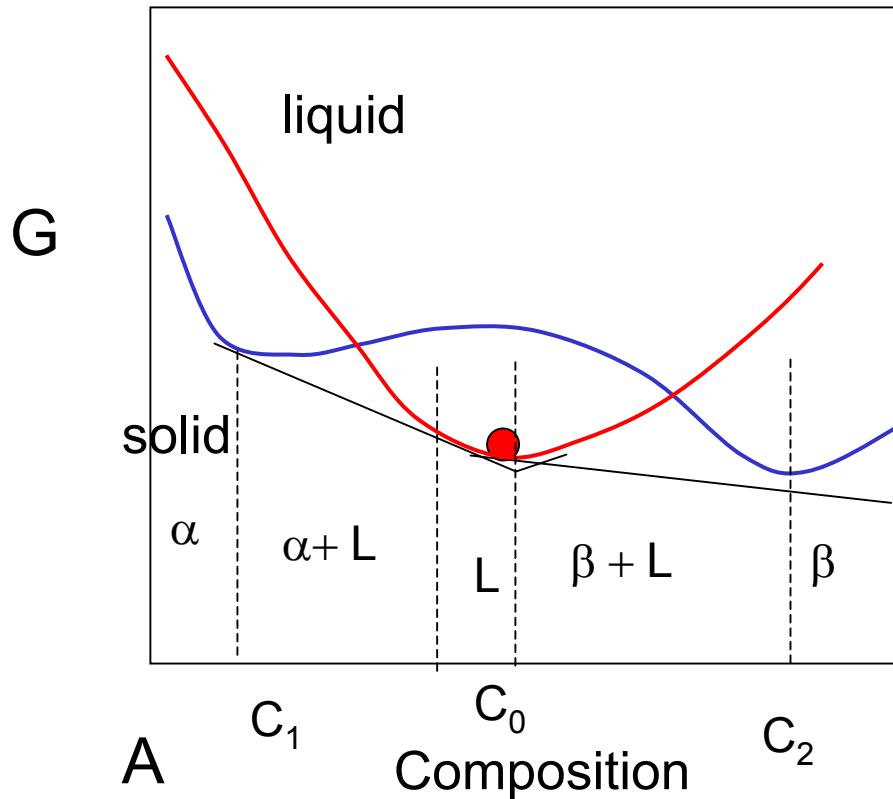


For a particular temperature the free energy curve of the liquid has a common tangent to the line joining the minima

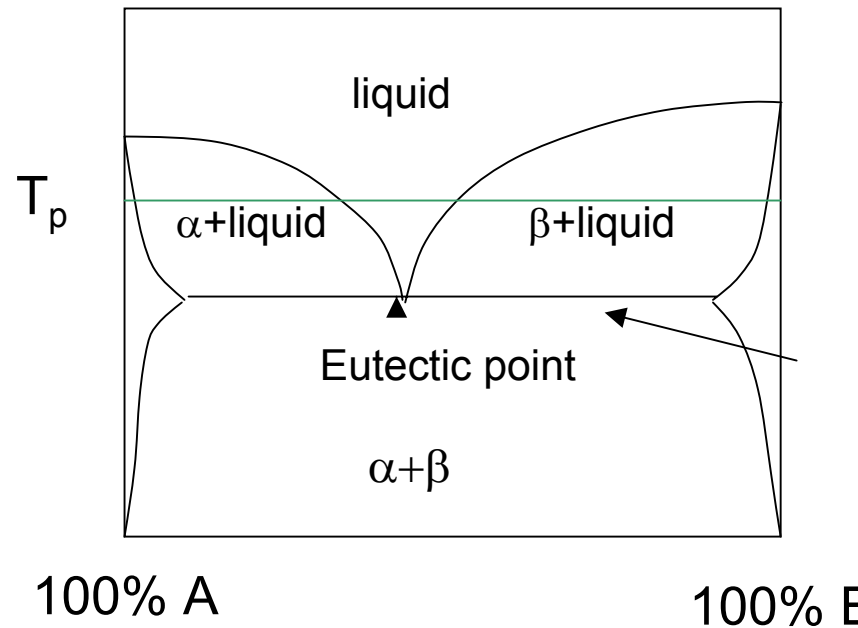
All 3 phases exist in equilibrium at the eutectic temperature

Liquid solidifies directly into 2 phases α and β

Free energy at general temperature



At a general temperature T_p
 2 minima have different
 tangents to the liquid curve

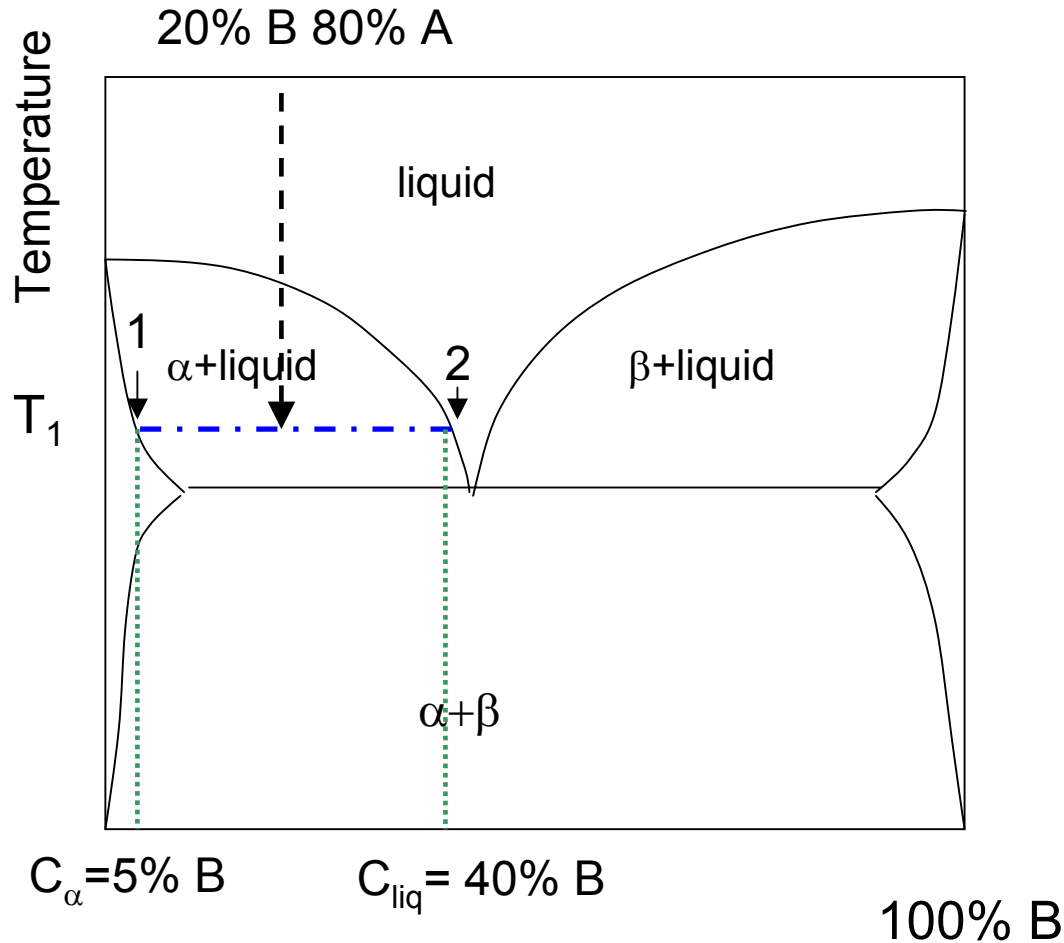


Eutectic

- Eutectic – means easily melted (Greek)
- Eutectic point – the bottom point of the V formed by 2 liquidus lines
- Eutectic line – the horizontal line running through the eutectic point
- The Eutectic reaction – a 3 phase reaction in which , on cooling, a liquid transforms into 2 solids



Phase Diagrams – Tie Lines



Cool liquid mixture

20% B 80% A to a temperature T_1

Draw horizontal line at this temperature

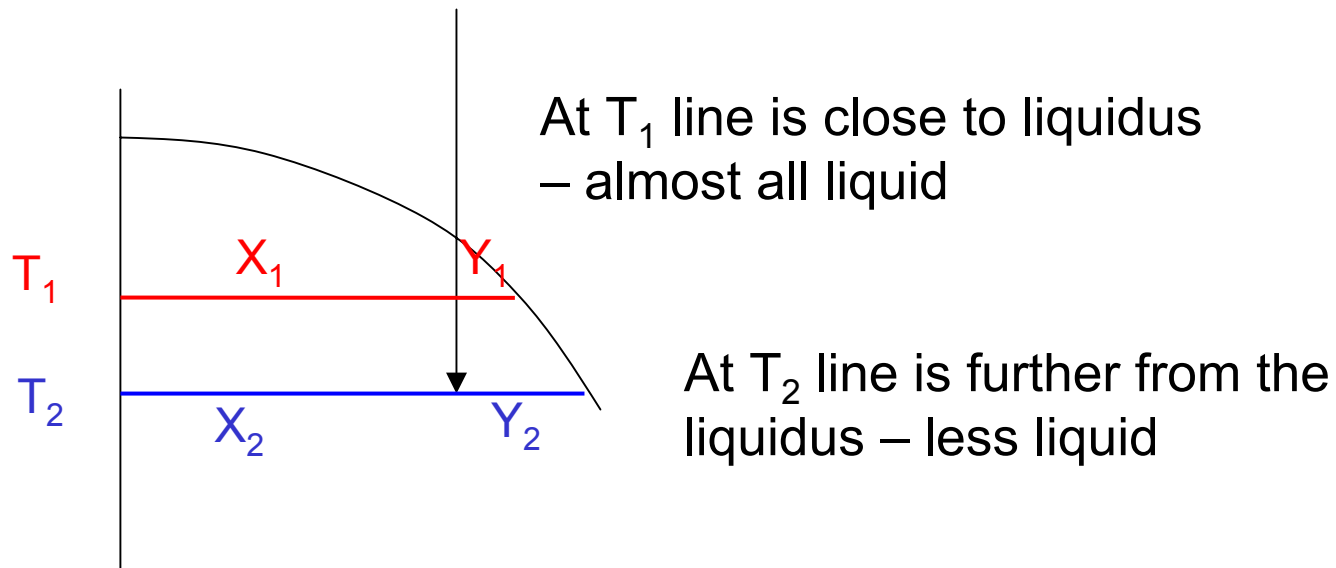
Line meets liquidus at 1 and solubility limit line at 2

At T_1 the composition of α is that corresponding to point 1 and the composition of the liquid corresponds to point 2

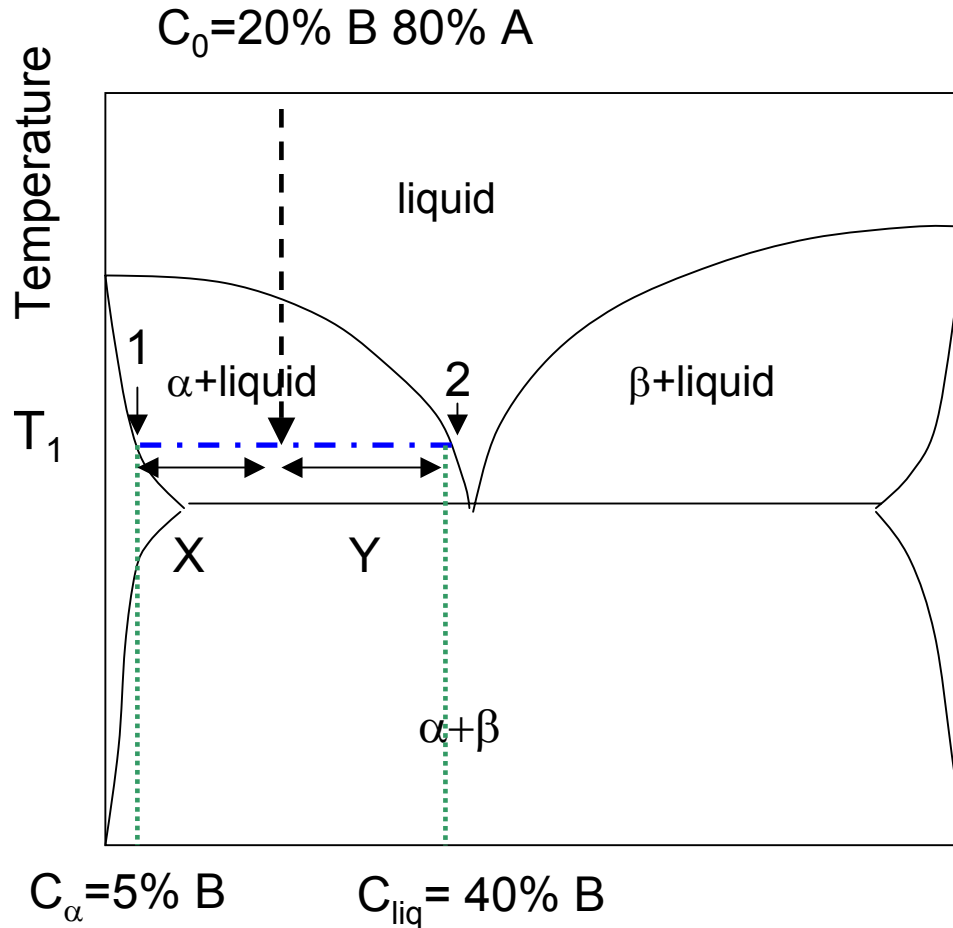
The Lever Rule

The relative amounts of each phase at a given temperature and composition is given by the relative lengths of the tie lines

For each phase use the line furthest from that phase



The Lever Rule - Proof



Conservation of mass

$$C_0 = f_\alpha C_\alpha + (1-f_\alpha) C_{\text{liq}}$$

Rearranging

$$f_\alpha = (C_{\text{liq}} - C_0) / (C_{\text{liq}} - C_\alpha)$$

$$(C_{\text{liq}} - C_0) = Y$$

$$(C_{\text{liq}} - C_\alpha) = X + Y$$

$$\text{So } f_\alpha = Y / X + Y$$

$$\text{And } 1 - f_\alpha = X / X + Y$$

Here $X = 15$; $Y = 20$

$$f_\alpha = 20 / 35$$

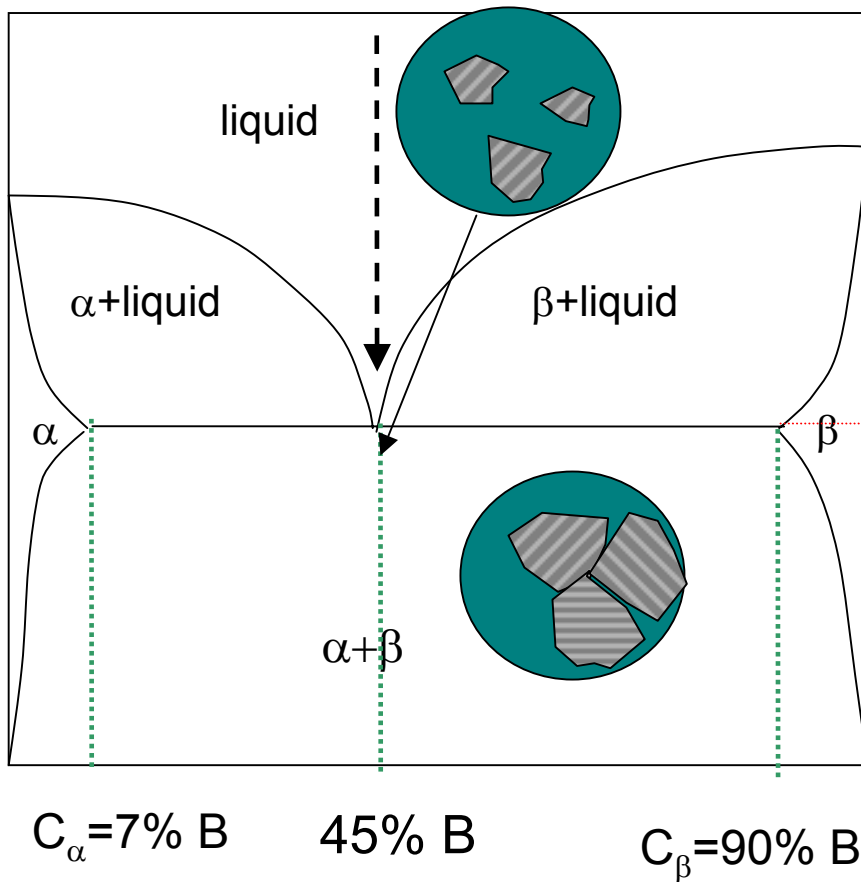
$$1 - f_\alpha = 15 / 35$$

Case Study – Solder (Ashby)

Type	Composition	Melting Range	Uses
Soft eutectic (free flowing)	62 Sn 38 Pb	183	Electronic assemblies
Soft general purpose (moderately pasty)	50 Sn 50Pb	183-212	Plumbing joints sheet metal work
Soft Plumbers (pasty)	35 Sn 65 Pb	183-244	Wiped Joints car body filling
Soft High melting (free flowing)	5Sn 93.5 Pb 1.5 Ag	296-301	Higher temperatures

Eutectic Alloy

Cool liquid with eutectic composition ($C_e = 45\% \text{ B}$)



At T_e liquid starts to solidify at favourable nucleation sites

Alloy forms stripes of α and β phases – stripes often of the order of 1 micron thick

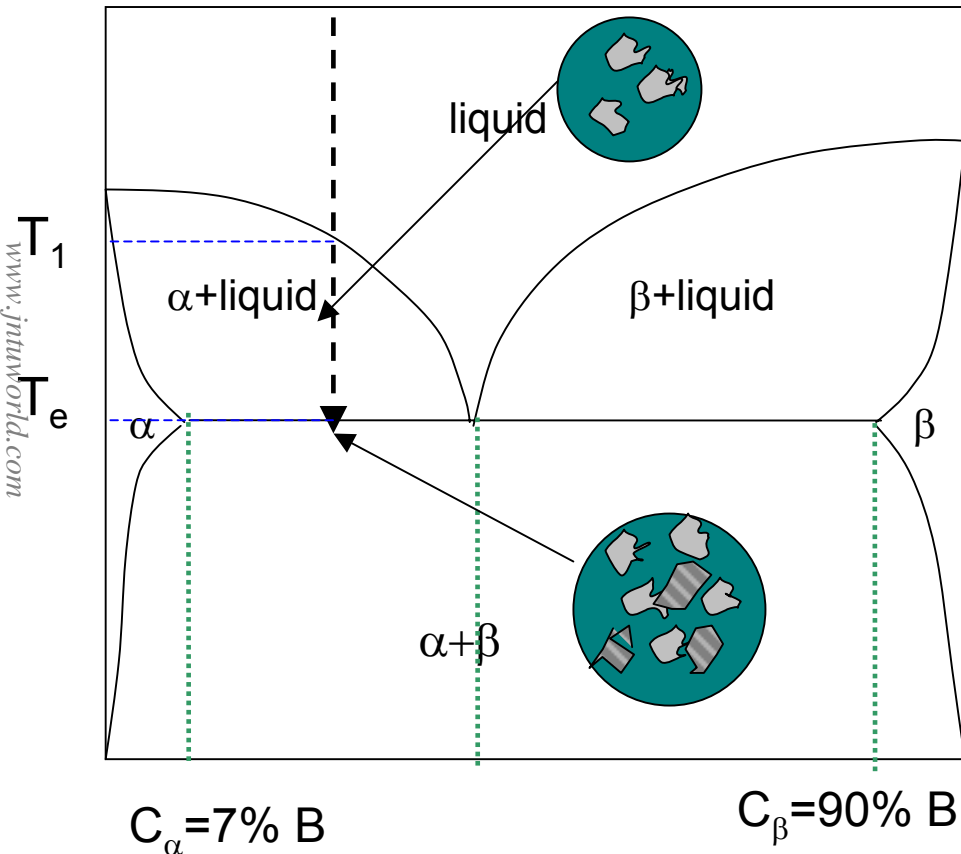
On further cooling nuclei grow adding α to α and β to β

Crystals eventually coalesce and form grain boundaries

Result polycrystalline metal with uniform composition

Hypo-eutectic Alloy

Cool liquid with composition to the left of the eutectic



At T_1 α phase nucleates

On further cooling a grains grow and liquid becomes rich in B

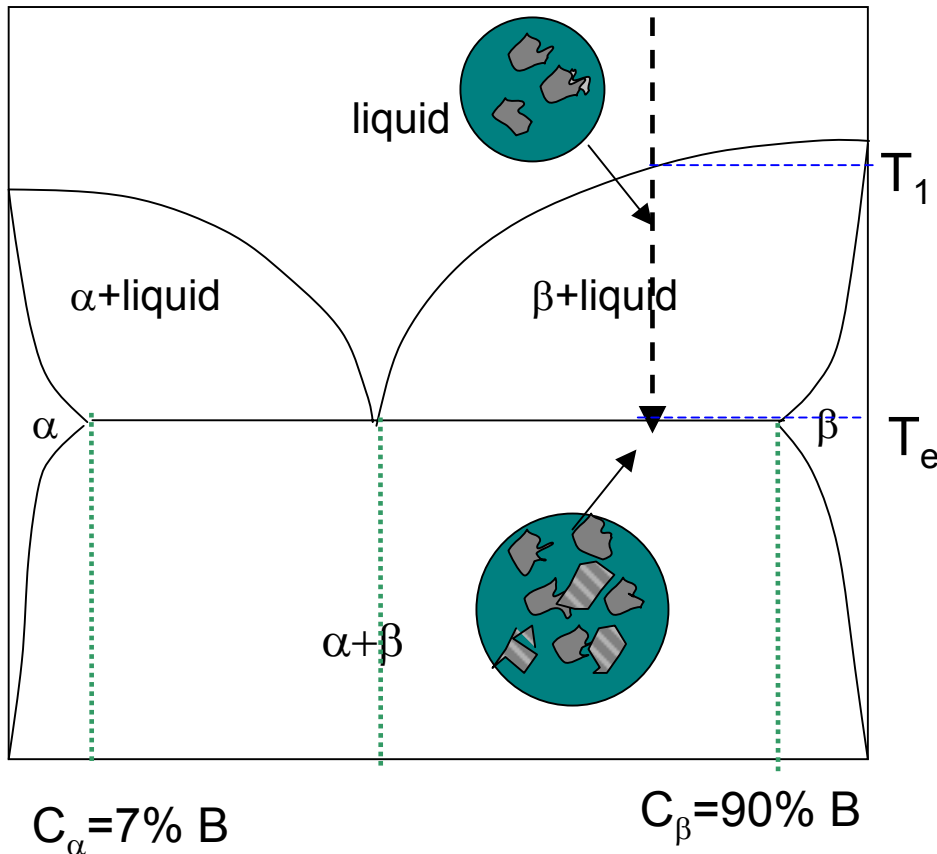
At T_e Remaining liquid has reached the eutectic composition

2nd phase grows – lamellar phase of α and β

Result polycrystalline metal with grains of α and grains of lamellar α and β

Hyper-eutectic Alloy

Cool liquid with composition to the right of the eutectic



At T_1 β phase nucleates

On further cooling grains grow and liquid becomes rich in A

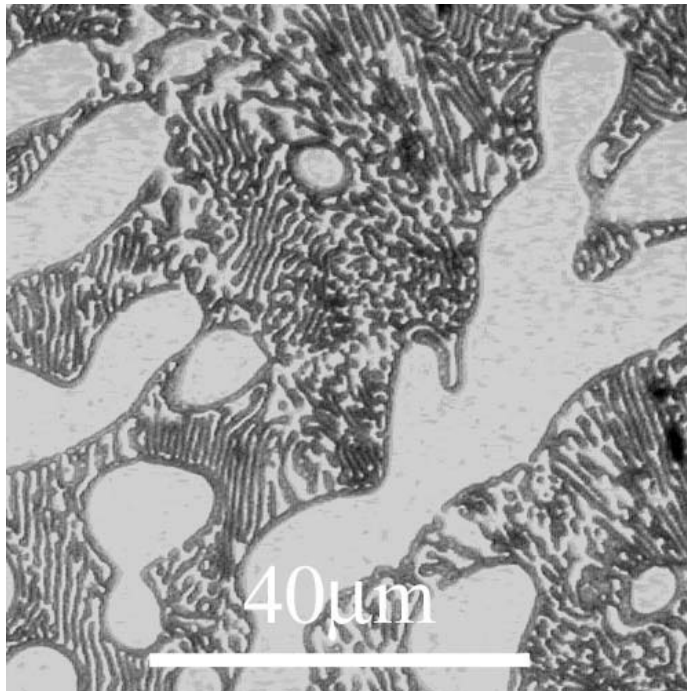
At T_e Remaining liquid has reached the eutectic composition

2nd phase grows – lamellar phase of α and β

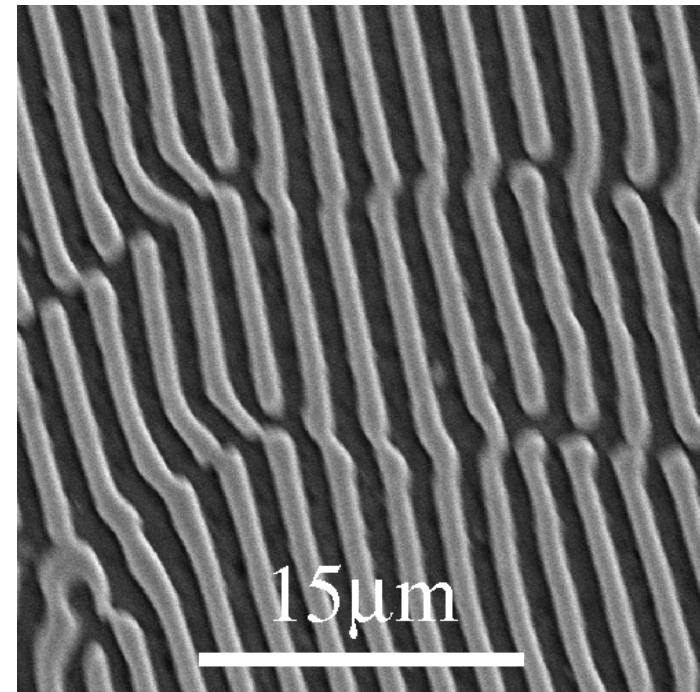
Result polycrystalline metal with grains of β and grains of lamellar α and β

Examples of Al Cu Microstructures

From www.msm.cam.ac.uk/doitpoms



Al_{0.75}Cu_{0.25} hypoeutectic
Reflected light microscope



Al_{0.67}Cu_{0.33} eutectic alloy
SEM

Complex Binary Phase Diagrams

- In some systems intermediate phases exist in which A and B form ordered structures (eg Brass CuZn)
- Intermetallic compounds between A and B are also possible
- Intermetallic compounds have distinct structures and chemical compositions (eg Mg_2Pb)
- Solid solutions between ordered and intermetallic compounds and other phases can exist, leading to complex phase diagrams

Invariant Points

- Invariant points involve 3 phases in equilibrium
 - Eutectic – 1 liquid and 2 solid
 - Eutectoid – 3 solid
 - Horizontal line known as eutectoid line or isotherm
 - Eutectoid reaction $\delta \rightarrow \gamma + \varepsilon$
 - Eutectoid structure is similar to eutectic but on a much finer scale
 - Peritectic – Solid + liquid transforms to solid
 - Peritectic reaction $\delta + L \rightarrow \varepsilon$

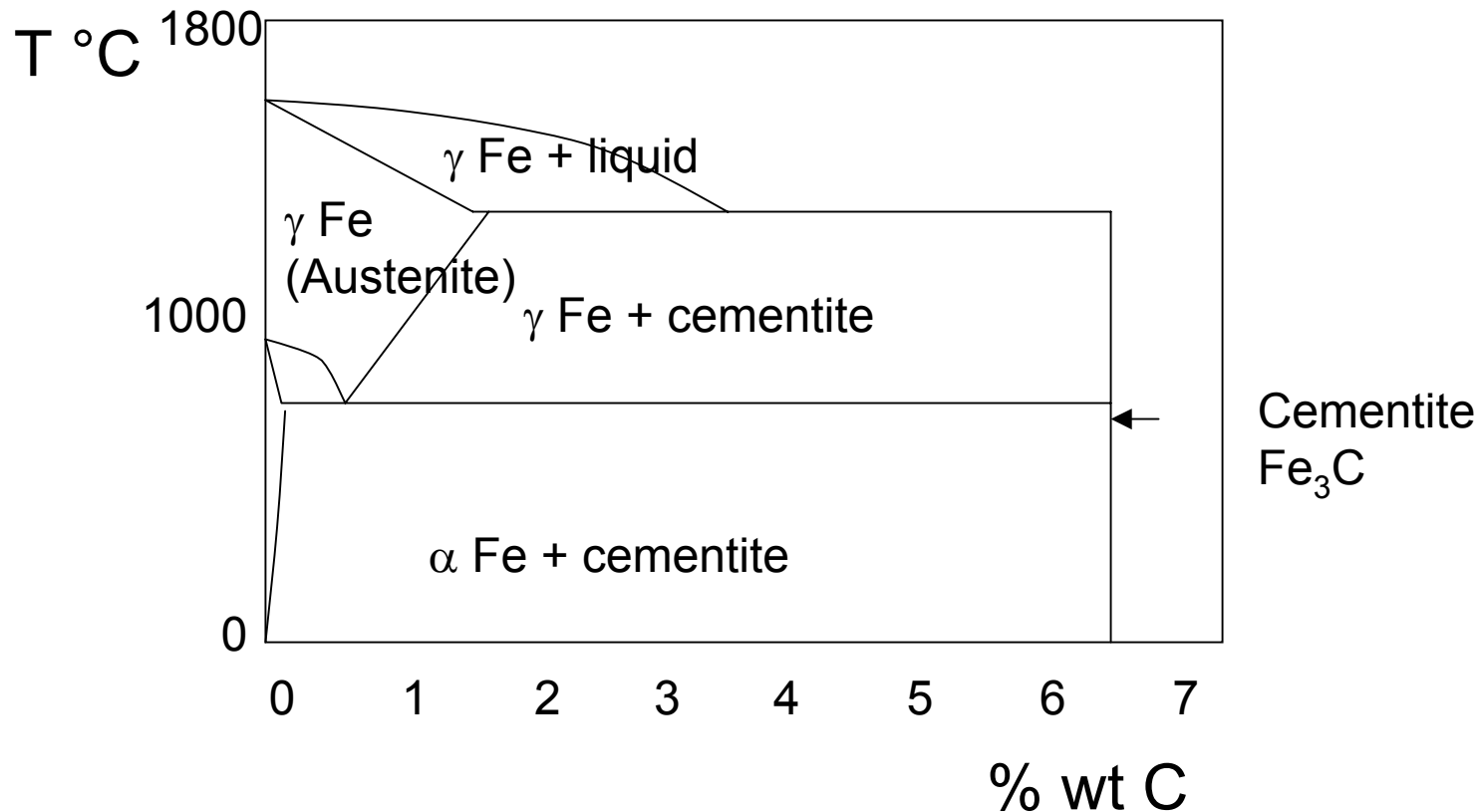
Fe / C System (Steel)

Pure Fe

Room T BCC α iron ferrite

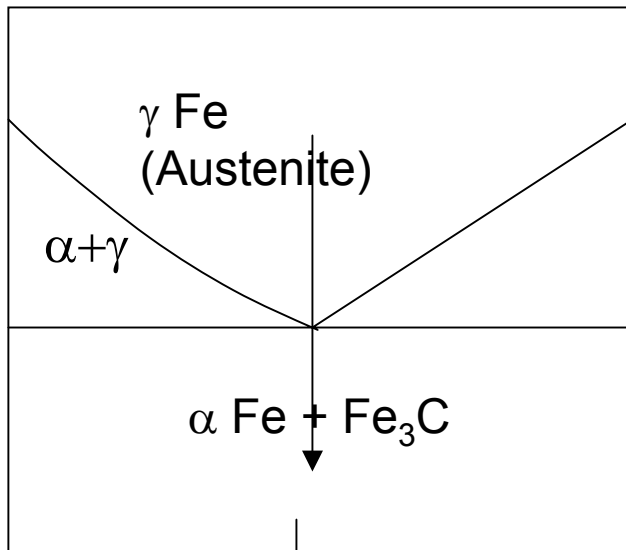
> 912 C FCC γ iron Austenite

> 1394 C BCC δ ferrite

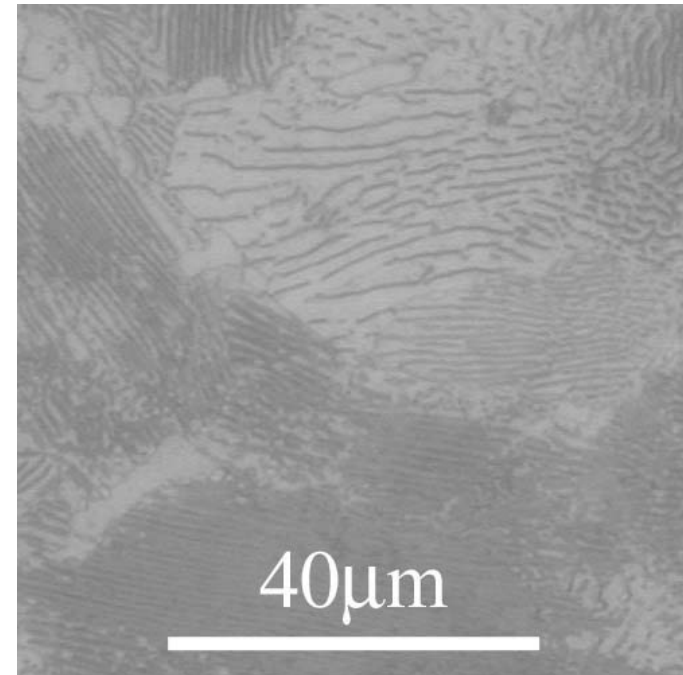


0.8% C Steel - eutectoid

Pearlite



0.8% C



Lamellar structure – tough
microstructure controlled by cooling rate

Phase Transformations - Kinetics

- Development of microstructure involves phase transformations – an alteration of the number and/or character of the phases
- Three types of transformation
 - Diffusion dependant with no change in number or composition of phases (eg solidification of pure metal)
 - Diffusion dependant with a change in number and/or composition of phases (eg eutectoid)
 - Diffusionless – metastable state produced (eg Martensite)

Avrami Equation

The fraction of transformation (y) at time t is given by

$$y = 1 - \exp(-kt^n)$$

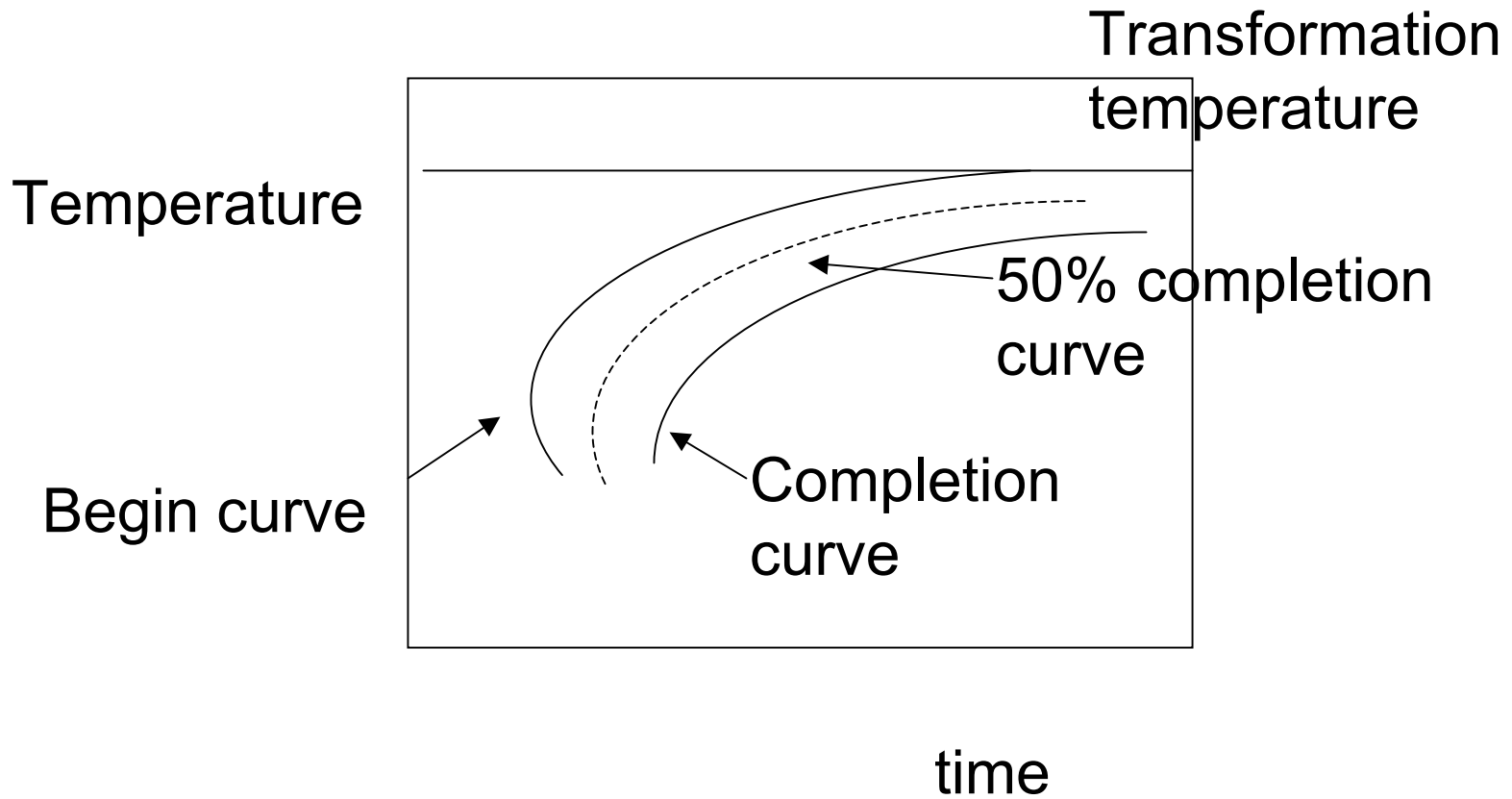
The rate of a transformation (r) is taken as the reciprocal of the time for the transformation to proceed half-way to completion

$$r = 1/t_{0.5}$$

For thermally activated reactions

$$r = A \exp(-Q/kT)$$

TTT Plots



Steel

- Probably the most important engineering material
 - Structures – buildings, bridges
 - Transport – trains, cars, ships
 - Tools – screw drivers, cutting tools, knives
 - Architecture
- Very versatile - properties controlled by heat treatment and alloying

Types of Steel

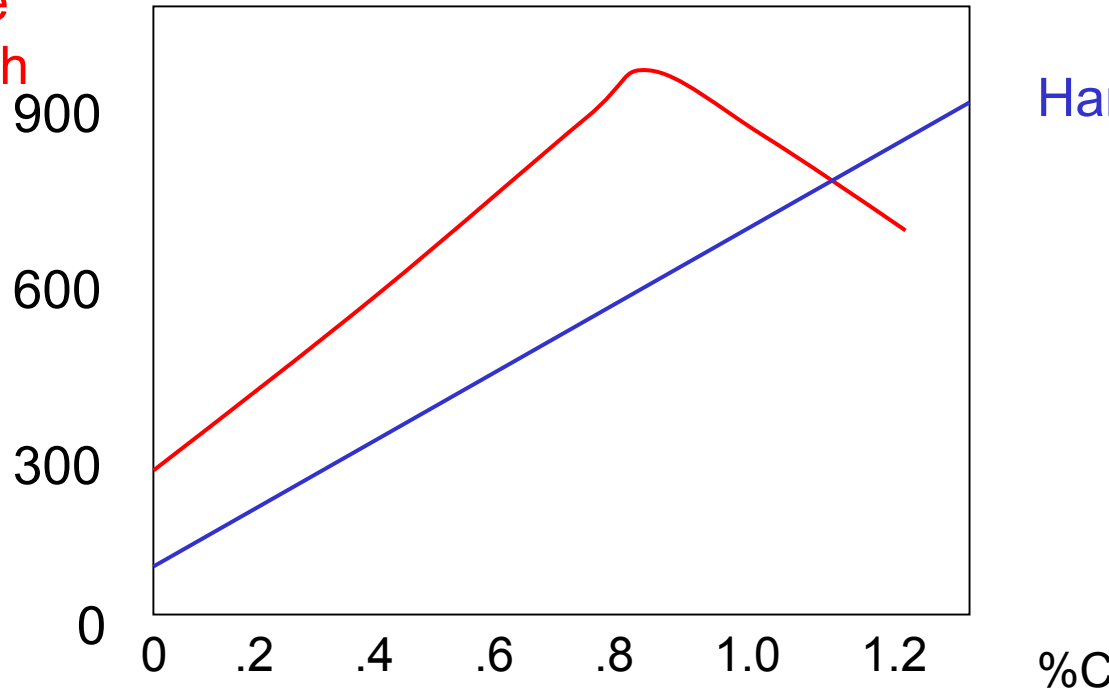
- Carbon steel
 - Low carbon $< 0.1\%$ C
 - Medium carbon $< 0.25\%$ C
 - High carbon
- Alloy steels
 - Co, Ni, Mo, Ti, V, Nb, Al in varying amounts
- Stainless steels
 - Cr gives good corrosion resistance

Phases

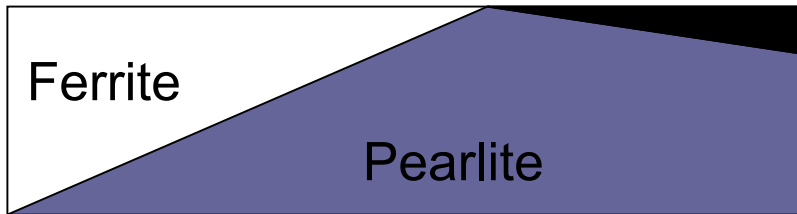
- Ferrite (α steel) bcc – limited solubility of C
- Ferrite (δ steel) bcc – only relevant at very high T
- Austenite (γ steel) fcc – high solubility of C
- Cementite Fe_3C – orthorhombic (6.67% wt C)
- Pearlite – eutectoid intergrowth of ferrite and cementite

Carbon Steels - Properties

Tensile strength
MPa

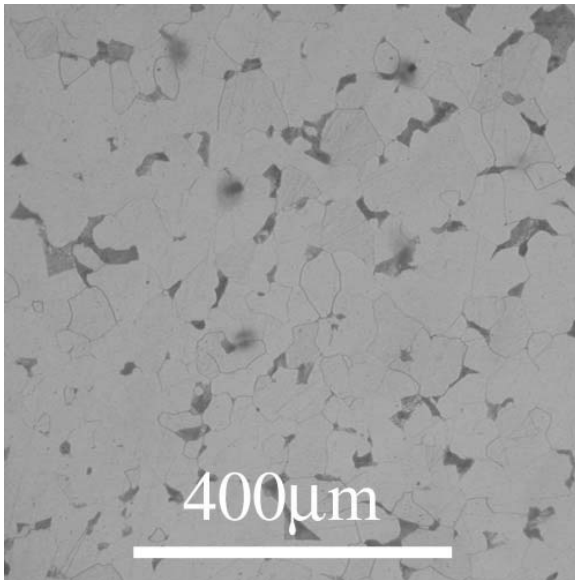


Hardness



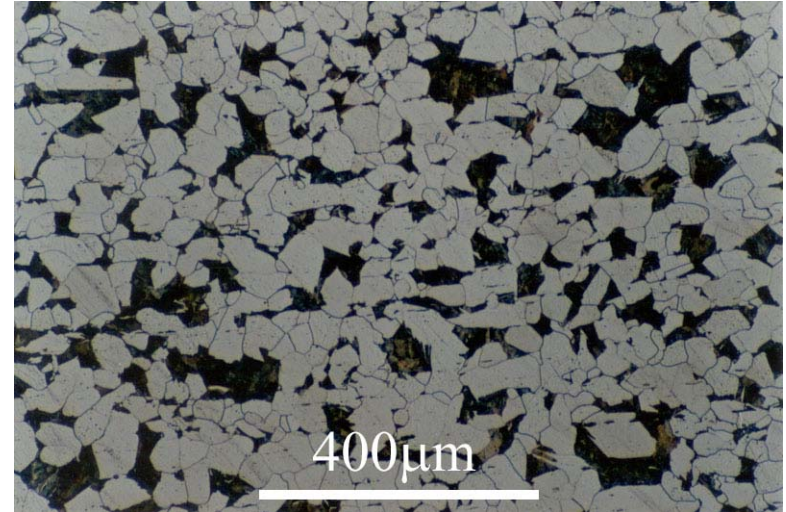
Cementite

Micrographs

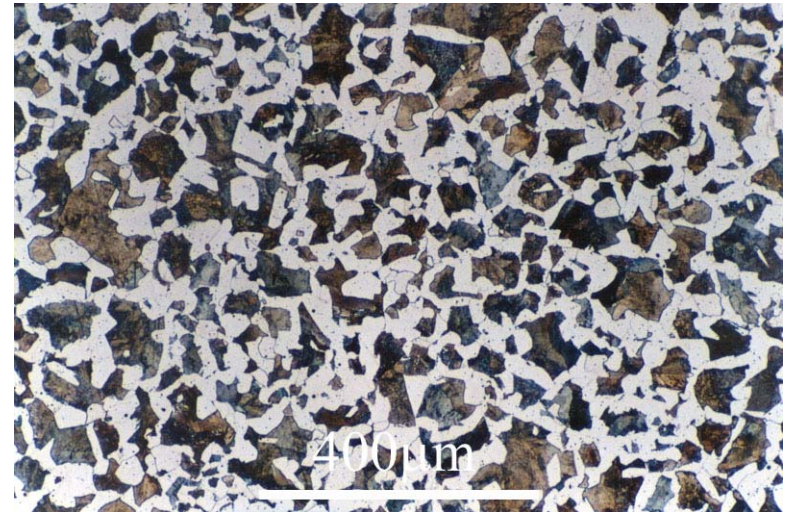


0.1% C

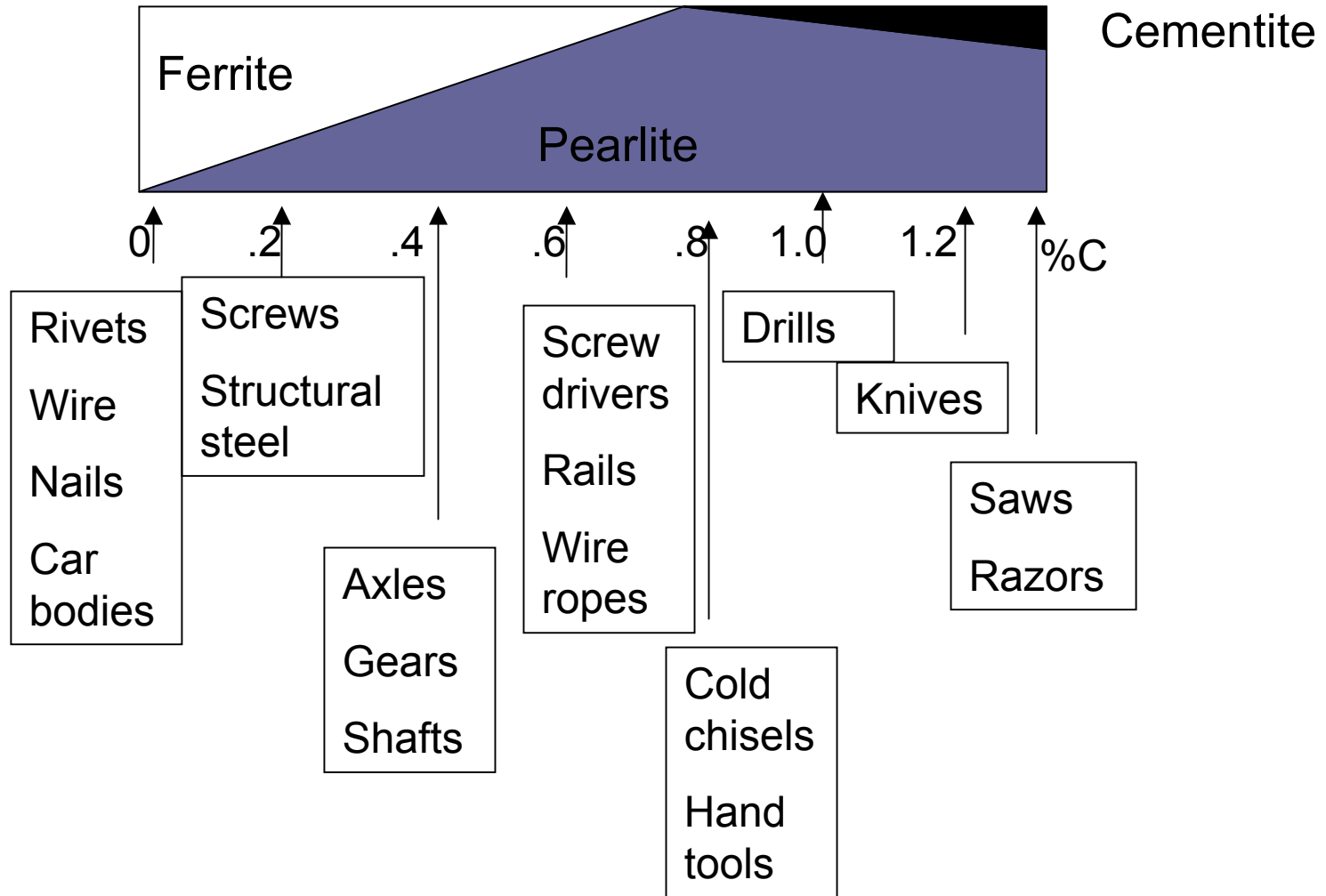
0.2% C



0.4% C



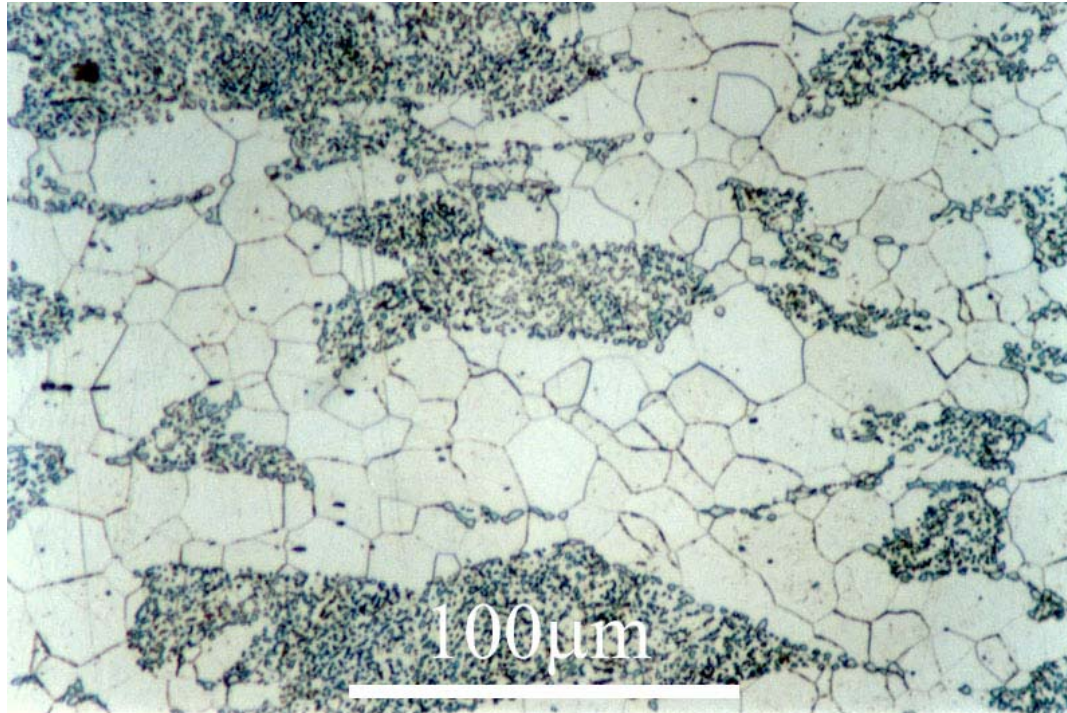
Carbon Steels - Uses



Carbon Steels

- Spheroidite
 - Formed by holding pearlite at 700 C for 18 – 24 hours
 - Fe₃C particles form spheres in ferrite matrix
 - Reduces high energy phase boundaries
- Bainite
 - Formed by cooling austenite between 200 C and 500C
 - Thin needles of ferrite separated by elongated particles of cementite
- Martensite
 - Non-equilibrium single phase (bcc) resulting from quenching from austenite (fcc)
 - High residual stress

Spheroidised Steel

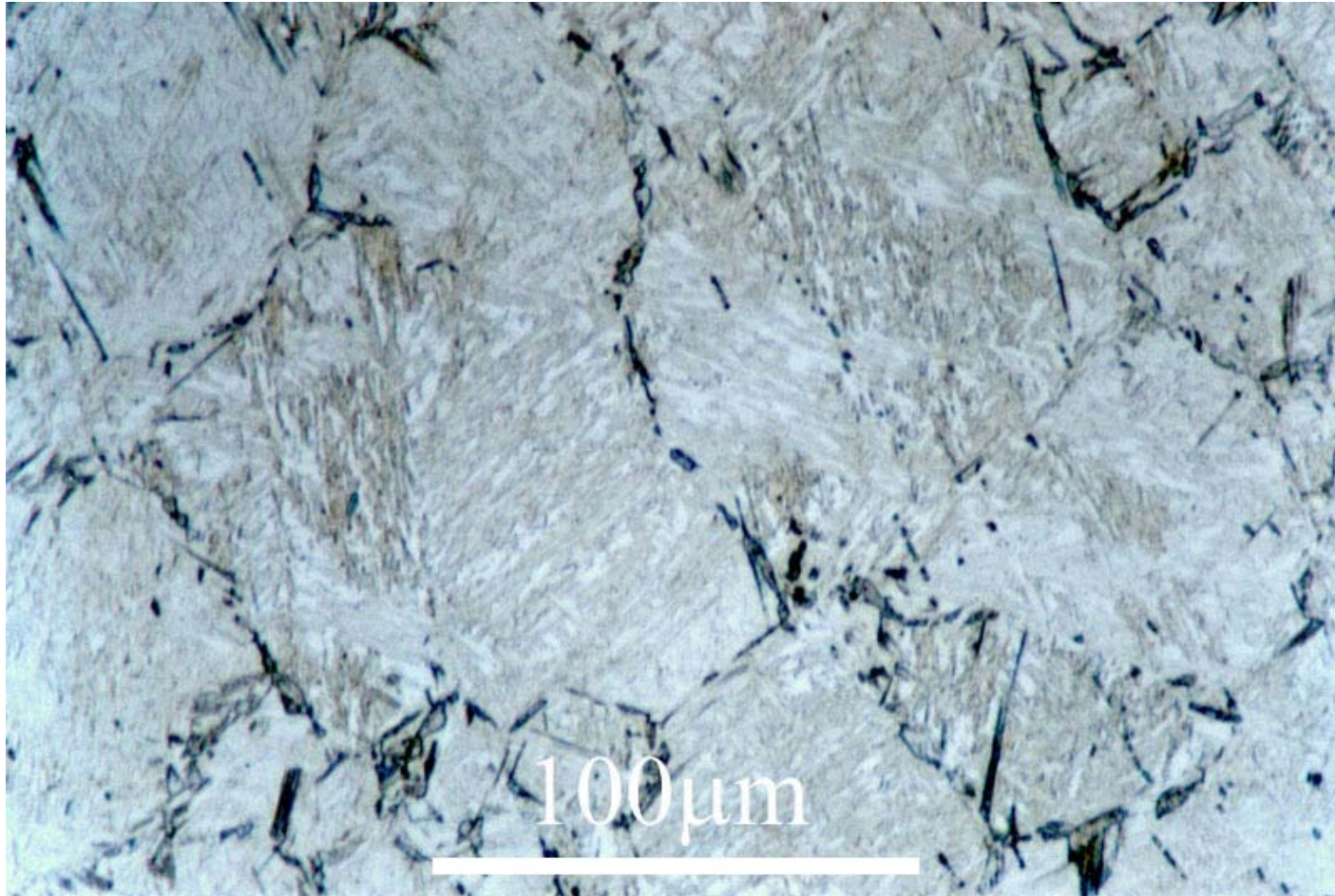


0.3% C annealed just below the transformation temperature.

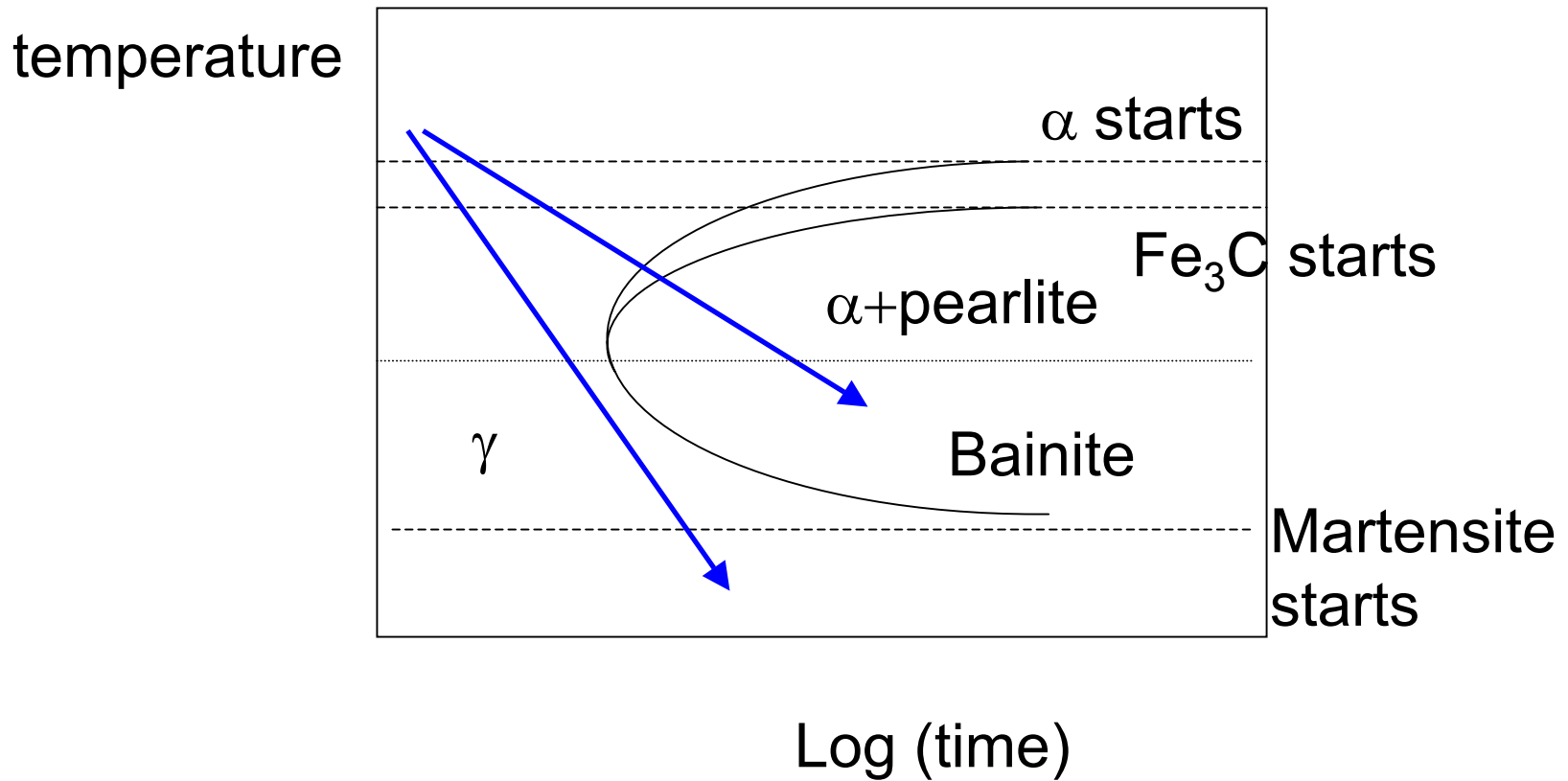
Cementite forms spherical particles

Softer and more ductile than pearlite

Bainite - Microstructure



TTT Plot



Quenched Steels - Martensite

γ is supercooled too fast for α to nucleate

γ is well below transformation T but diffusion is slow. C is stuck in supersaturated solution

At Martensite temperature driving force is large enough to nucleate α – but with trapped C atoms

The trapped C atoms distort the bcc unit cell of the α phase in 3 possible directions

The distorted cells lock in large stresses

Displacive vs Diffusive Transformations

Displacive

Atoms move < interatomic distance

Atoms move in precise sequence

Speed ~ velocity of sound

Extent of transformation depends on T (not time)

Composition cannot change

Diffusive

Atoms move $1-10^6$ interatomic distances

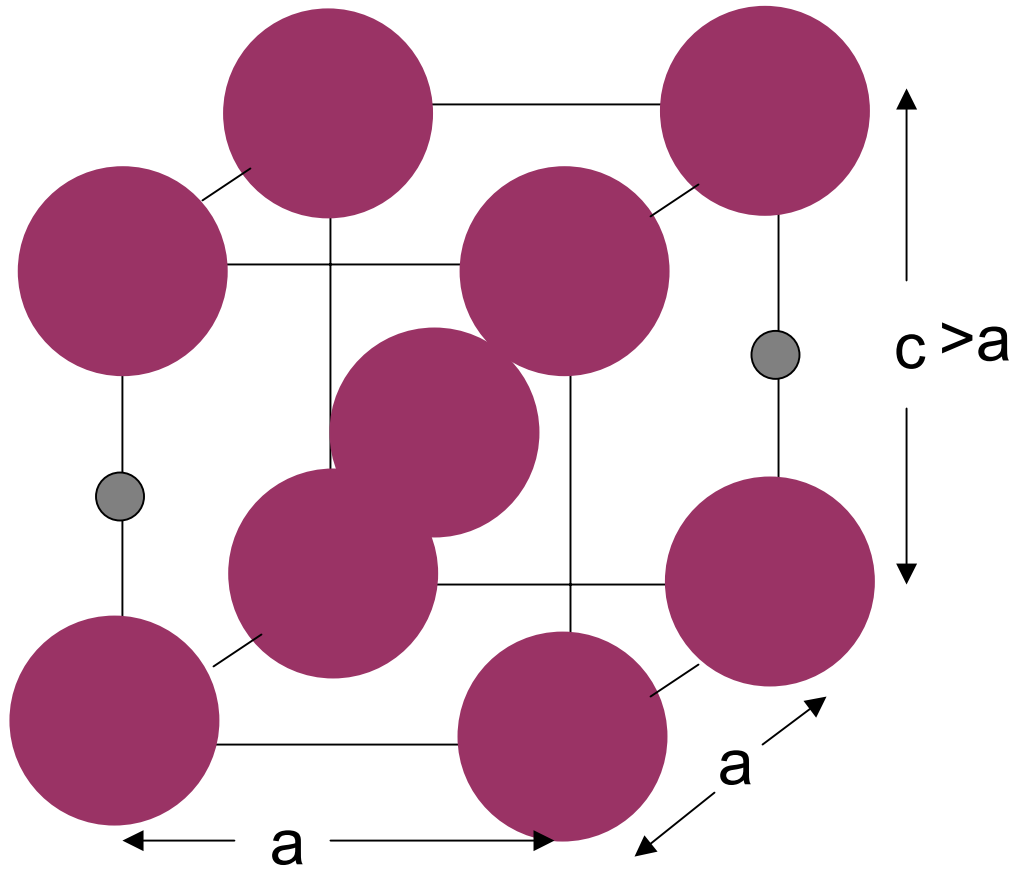
Atoms move randomly by hopping from site to site

Speed of transformation depends on temperature

Extent of transformation depends on time and T

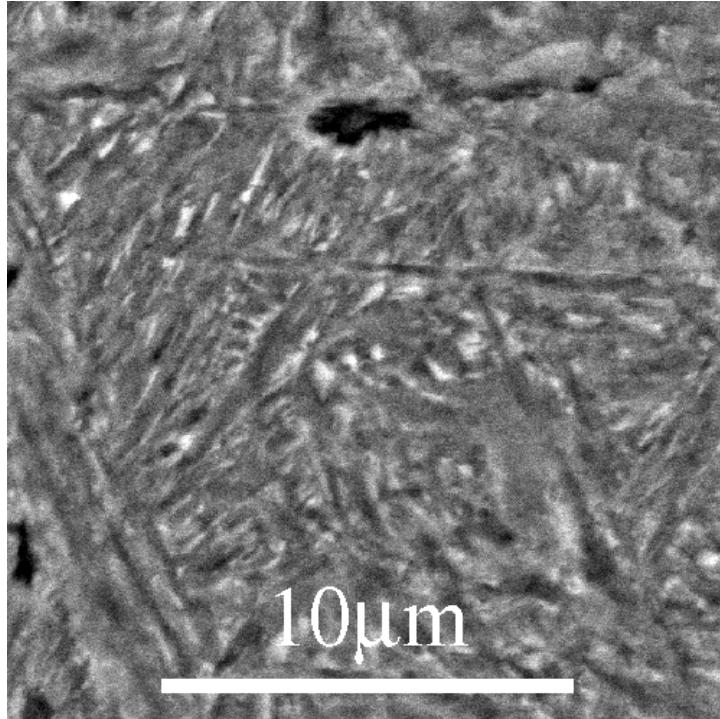
Composition of phases can change

Martensite - Structure

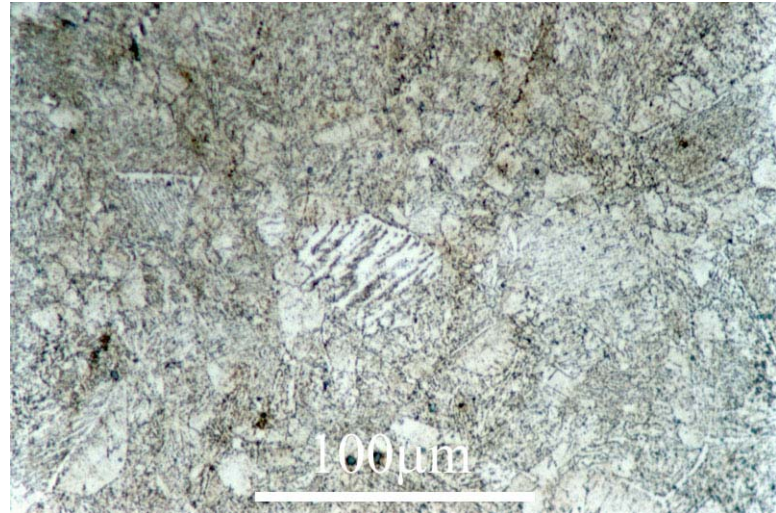


Distorted BCC

Martensite - microstructures



Fe, C 0.9 (wt%) steel,
Water quenched from 800 °C



Fe, C 0.75 (wt%) steel,
quenched and tempered

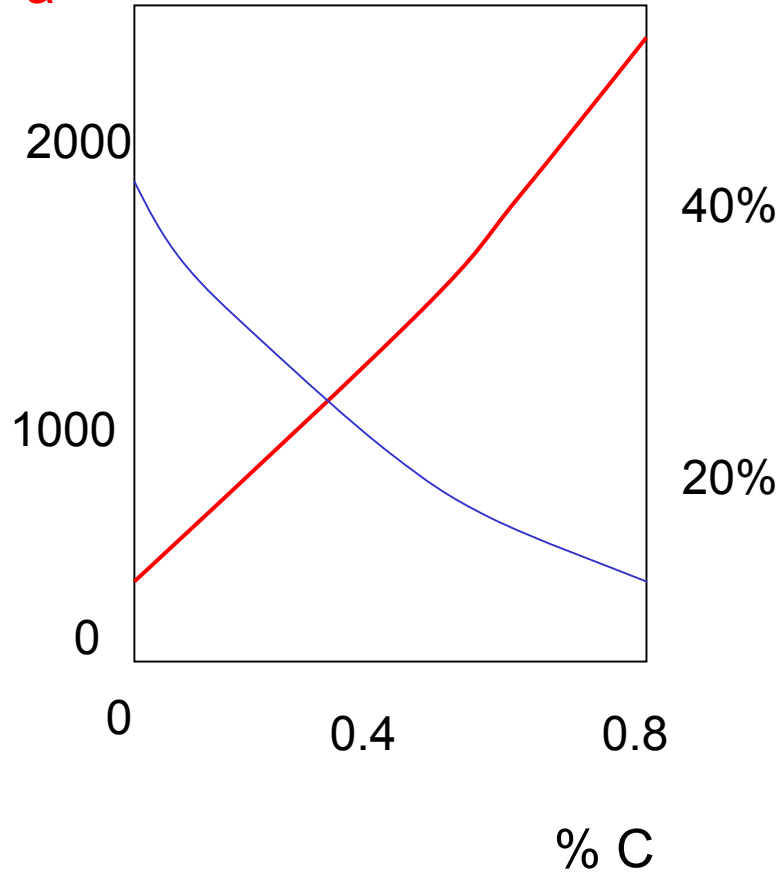
Martensite - properties

- As quenched martensite is very hard and brittle
 - Many interfaces and strongly varying local stresses
 - Very high resistance to dislocation motion
- Tempering increases ductility and toughness
 - Low temperature $< 350\text{ }^{\circ}\text{C}$ - C precipitates as Fe_3C and internal stresses disappear
 - Moderate temperatures $350^{\circ}\text{C} < T < 500\text{ }^{\circ}\text{C}$ – C precipitates as Fe_3C
 - High temperature $T > 500\text{ }^{\circ}\text{C}$ Fe_3C particles coarsen and become more widely spaced

Mechanical Properties

Strength
MPa

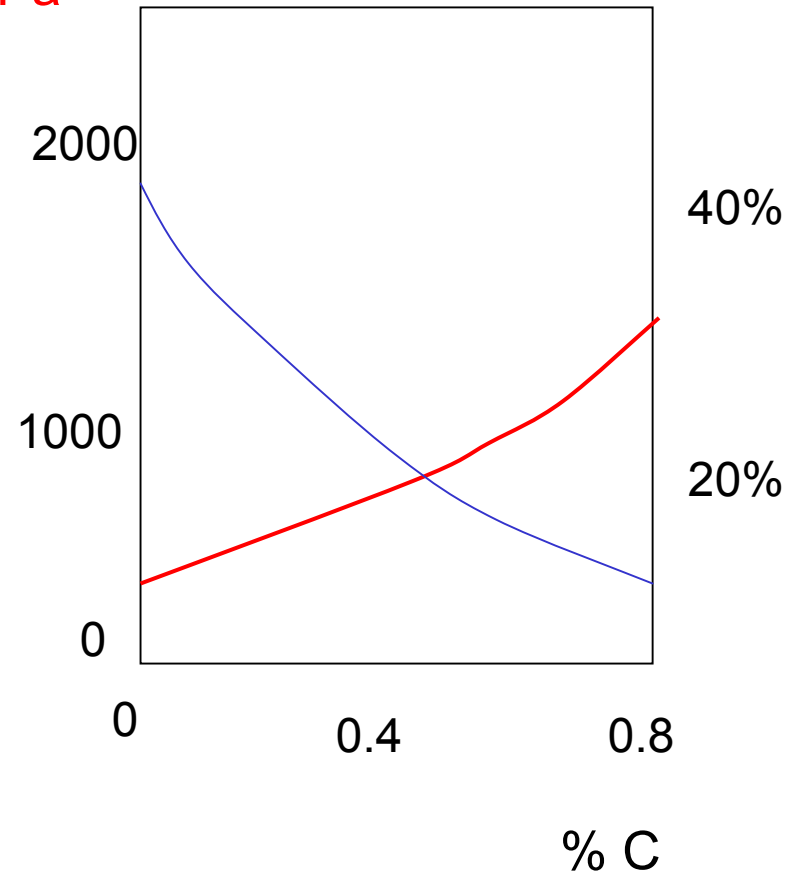
Ductility



Quenched and tempered steel

Strength
MPa

Ductility



Normalized steel

Alloy Steels

- Alloying elements added to steel to
 - Improve hardenability
 - Alloying increases the CCR permitting the formation of martensite with slower cooling
 - Give solution strengthening and precipitation hardening (Si, Mn)
 - Give corrosion resistance (Cr)
 - Stabilize austenite (Ni)

Stainless steels

- Based on Fe-Cr-Ni system
- 12% Cr forms tenacious oxide film
- Ni stabilises fcc γ phase
- Cr stabilises bcc α phase less strongly
- Types
 - Ferritic
 - Martensitic
 - Austenitic

Types of Stainless Steel

- Ferritic
 - 13% Cr 0.45% Mn <0.05% C
 - Poor mans stainless steel
 - UTS~500 MPa $\sigma_y \sim 350$ MPa $\epsilon_F \sim 30\%$
 - Cutlery, sinks
- Martensitic
 - 13% Cr 0.5% Mn 0.3% C
 - Quench from 1000 C, temper at 150-400 C
 - UTS~1500 MPa $\sigma_y \sim 1100$ Mpa
 - Sharp edged tools and springs
- Austenitic
 - 18% Cr 8% Ni <0.1% C
 - γ phase stabilised at room T by Ni
 - $\sigma_y \sim 550$ MPa $\epsilon_F \sim 40\%$ ductile, good creep resistant
 - Chemical industries (vats, pipes) Structural parts, decorative work

Steel - Summary

- Steel is the most common engineering material
- A wide variety of properties can be obtained by additives and processing
- Adding carbon to Fe increases toughness
- Adding Cr to Fe increases corrosion resistance

Light alloys

- Light alloys are those with a density $< 4.5 \text{ Mg m}^{-3}$
- 14 pure metals fall into this category but most are not widely used because they are
 - Too chemically active
 - Melting point is too low
- 3 important light metals
 - Aluminium – use exceeds all other metals apart from Fe
 - Magnesium
 - Titanium
- Stiffness to weight ratio and strength/weight ratio of all 3 are superior to steel
- Original usage confined to the aerospace industry – now their use is widespread and growing at 7% per annum

Properties of Light metals

Metal	Density (Mg m ⁻³)	T _m (°C)	Comments
Titanium	4.50	1667	Excellent creep resistance
Yttrium	4.47	1510	Good strength+ ductility, scarce
Scandium	2.99	1538	Scarce
Aluminium	2.70	660	
Strontium	2.60	770	Reactive in air/water
Beryllium	1.85	1287	Difficult to process, very toxic
Calcium	1.54	839	Reactive in air/water
Sodium	0.97	98	Very reactive in air/water
Potassium	0.86	63	Very reactive in air/water
Lithium	0.53	181	Very reactive in air/water

Mechanical Properties of Light Alloys

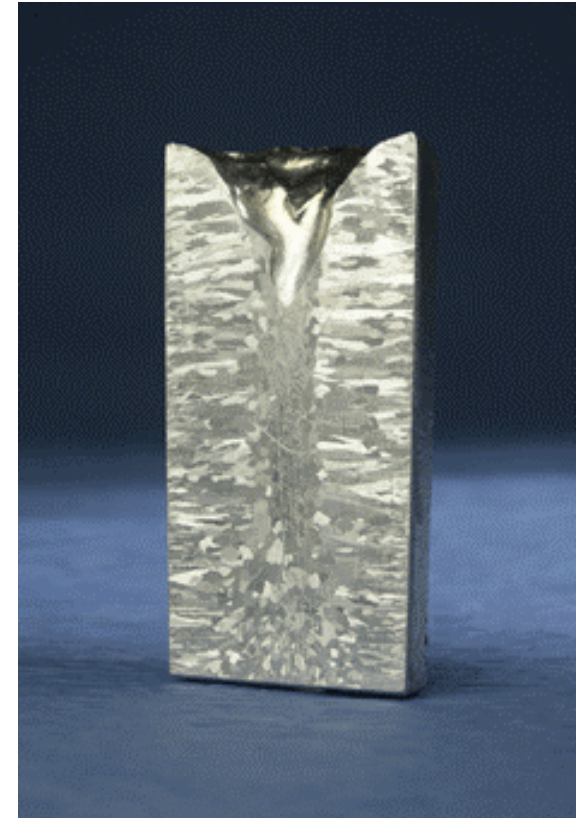
Alloy	Density ρ (Mg m ⁻³)	Young's Modulus E(GPa)	Yield σ_y (Mpa)	E/ ρ	E ^{1/2} / ρ	E ^{1/3} / ρ	σ_y/ρ	Creep Temperature (°C)
Al alloys	2.7	71	25-600	26	3.1	1.5	9-220	150-250
Mg alloys	1.7	45	70-270	25	4.0	2.1	41-160	150-250
Ti alloys	4.5	120	170-1280	27	2.4	1.1	38-280	400-600
(steel)	7.9	210	220-1600	27	1.8	0.75	28-200	400-600

Aluminium Alloys - Uses

- Construction
 - Window frames
 - Doors
- Packaging
 - Drinks cans
 - Al foil
- Transport – weight saving leads to fuel efficiency
 - Cars – from components to complete chassis
 - Boats (QE 2)
 - Aircraft
- Electrical
 - Power lines – reduced weight compensates for lower conductivity (60% of Cu)

Aluminium Alloys - Properties

- Light $\rho=2.702 \text{ Mg m}^{-3}$
- Low modulus/ high specific modulus $E= 71 \text{ GPa}$
- Low strength –improved by alloying
- Low fatigue strength
- Excellent corrosion resistance
 - Forms a thin protective (insulating) coating on exposure to air
- Good thermal and electrical conductor
- Good machining properties
- Ductile at low T (fcc)

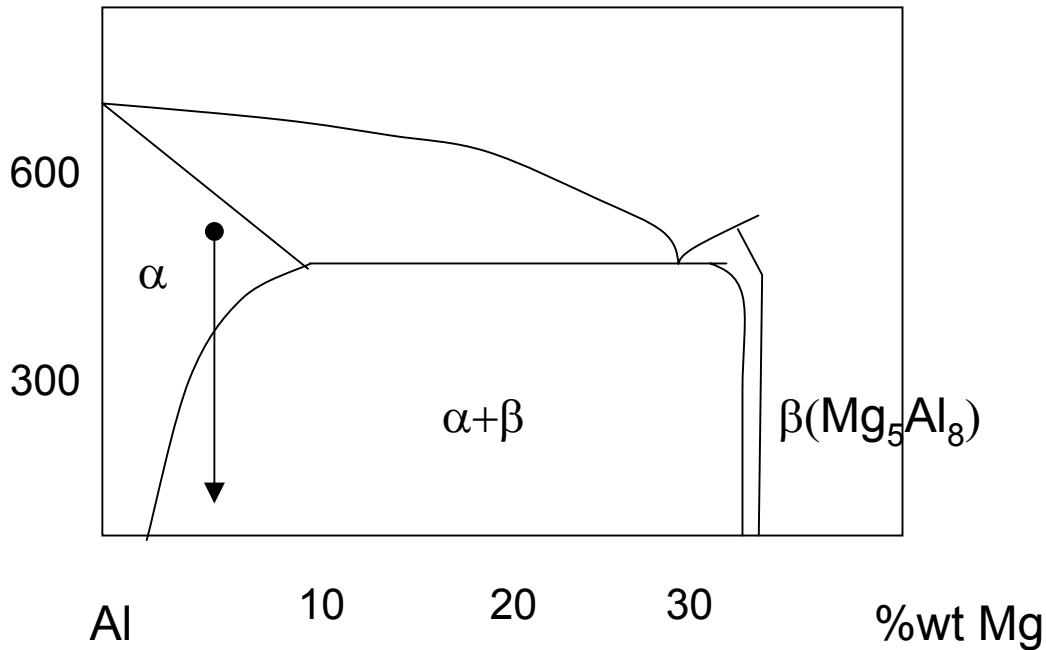


Pure Al forged – grain growth in direction of cooling front

Aluminium Alloys

Main Additions	Strengthening	Main Applications
None	None	Foil, Electrical
Cu	CuAl_2	Aircraft wings
Mn	Work hardened	General purpose, cookware
Si	Si needles	Casting alloy
Mg	Work hardened	Common, structural and boats
Zn Mg	ZnMg_2	High strength alloy
Li	Li_3Al	Low density - aircraft

Al/Mg Alloys



High solubility of Mg in Al

Hold at 450 C to dissolve 5.5% Mg

Cool rapidly to room temperature

Miss nose of TTT curve
– all Mg remains in supersaturated solution

Solution strengthening

Al Drinks Cans

- 8.5 Billion drinks cans manufactured in the UK each year
- 12% global Al output used for drinks cans
- Al suitable because it is
 - Light
 - Corrosion resistant
 - Ductile
- Alloy Al 1%Mg, 1%Mn, 0.4%Fe, 0.2%Si
- More Mg less Mn in cap



Design Requirements

- Minimise weight (transport costs)
- Minimise material
- Minimise joints
- Strength – must withstand
 - Manufacturing
 - Customers
 - 90 psi (3x car tyres pressure)
- Recycling can save 95% energy costs

Manufacturing method

- Circle cut from Al sheet
- Formed into shallow cup
- Ironed and punched to form final shape (0.25 mm thick)

Drawn and Ironed (DI) Cans

A

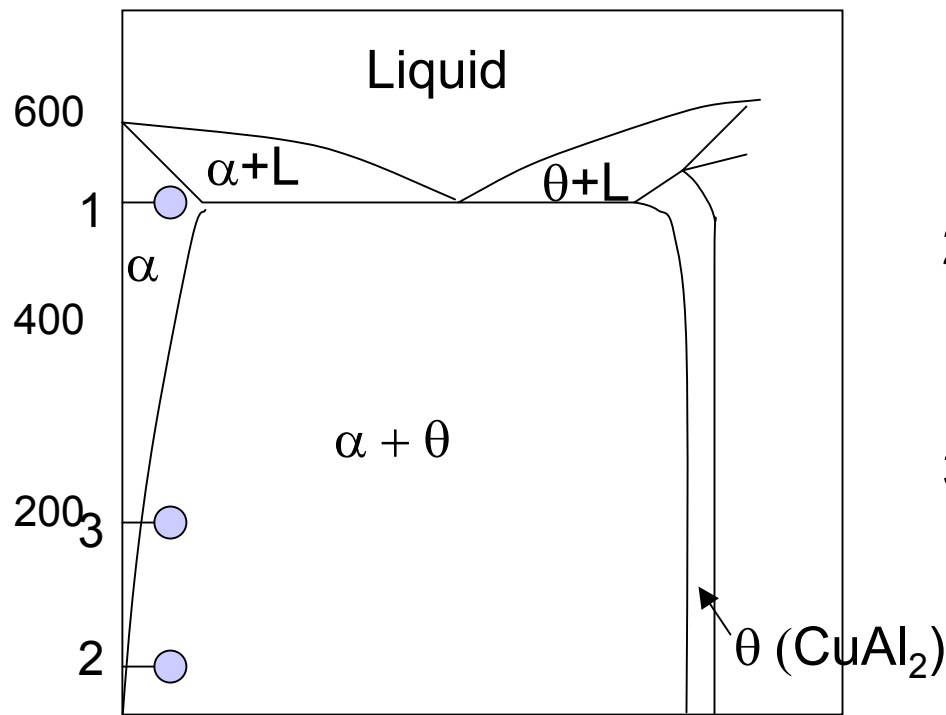


The DI cans are cleaned, decorated and lacquered at the customer plant prior to filling them with beverage.

Steel cans

- Steel cans 50% heavier than Al
- Dominate for cooked food
 - High pressure
 - High temperatures
- Corrosion can be a problem
 - Polymer coated steel
- Some have Al tops – recycling problem

Al – Cu Alloys (Duralumin)



4% Cu

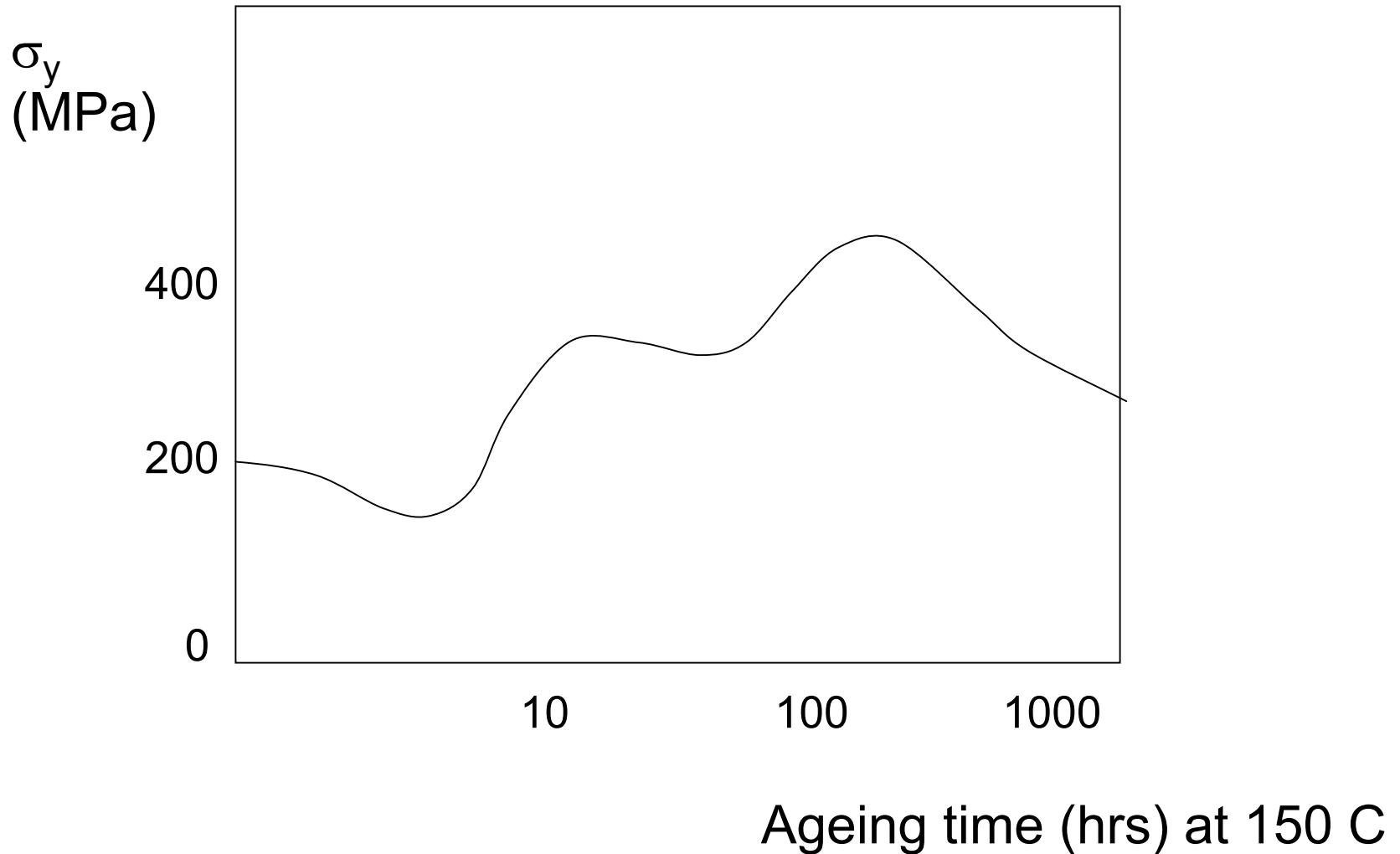
- 1 Hold at 550 C until all Cu is in solution
- 2 Quench to room T – supersaturated solution
- 3 Age at 200 C – CuAl_2 forms precipitates

[Quenching directly to aging temperature would cause precipitates to form at grain boundaries]

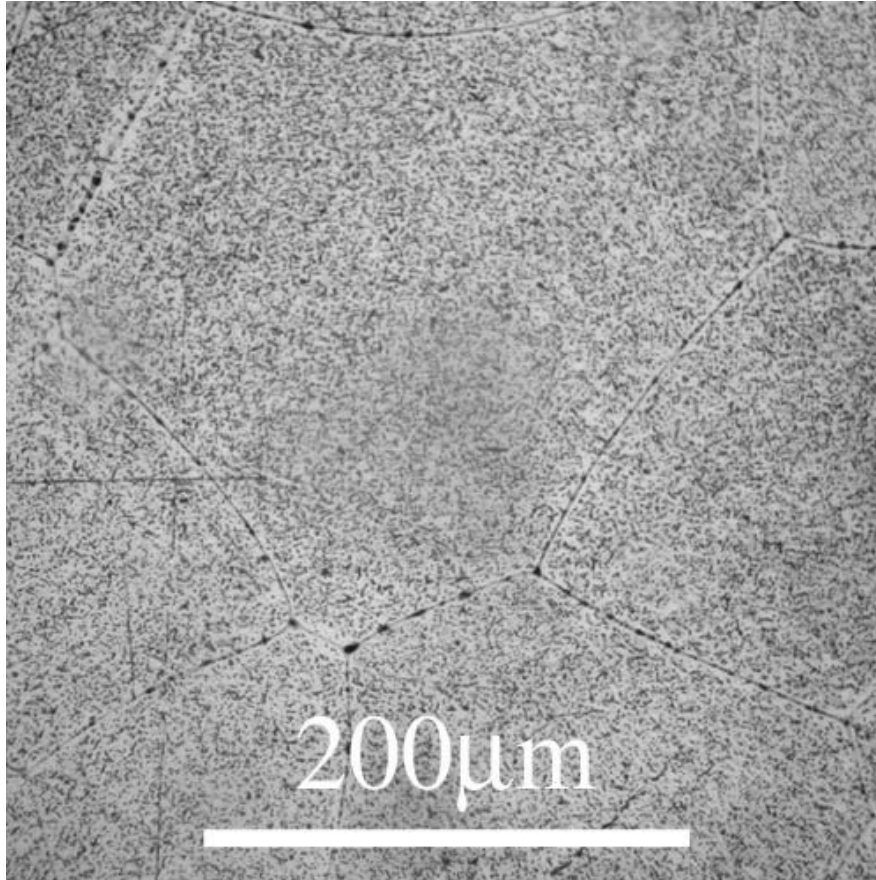
Age Hardening in Duralumin

- After quenching Cu dispersed randomly in supersaturated solution
- Initial stages of annealing leads to formation of single layer discs of Cu ~ 10 nm wide
 - Disc faces and edges coherent
 - Disc edges have coherency strain
- Further annealing leads to formation of θ'' phase 10 nm by 100 nm
 - Disc faces and edges coherent
 - Disc edges have coherency strain
- Further annealing leads to formation of θ' phase 100 nm by 10 μm
 - Disc faces and edges coherent
 - Disc edges incoherent
- AlCu_2 precipitates form – no coherency strain

Yield Strength vs Ageing Time



Al – Cu Alloys (Duralumin)



Al 96, Cu 4 (wt%),
solution treated and
overaged - precipitation
hardening

Magnesium Alloys - properties

- Lightest useable metal $\rho = 1.7 \text{ Mg m}^{-3}$
- Mg is 33% lighter but more expensive than Al
- Easier to cast and machine than Al
- Impact strength low
- Corrosion resistance very poor
 - anodise, chromate or coat with epoxy resin

Mg Alloys

- Al, Zn Th –precipitation hardening
- Mn – Corrosion resistance
- Zr – grain refinement

Ti Alloys

- 80% Ti produced used in aerospace industries
- Production – several hundred thousand tonnes per year (cf 750 million tonnes per year)
- Price would need to decrease by ~ 30% before used in mass-market cars

Titanium Alloys - Properties

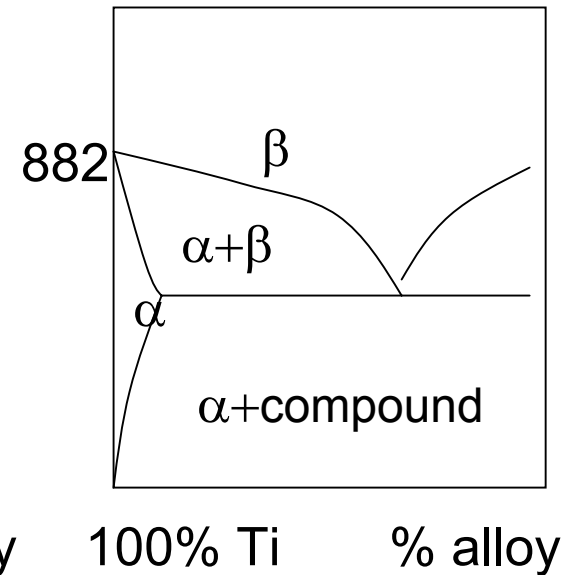
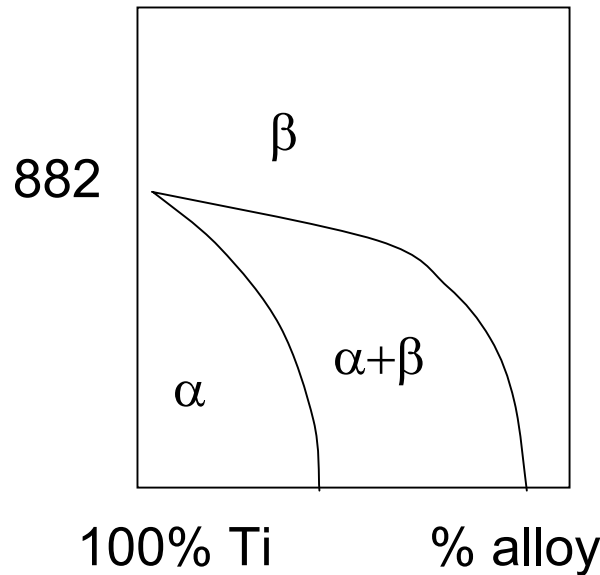
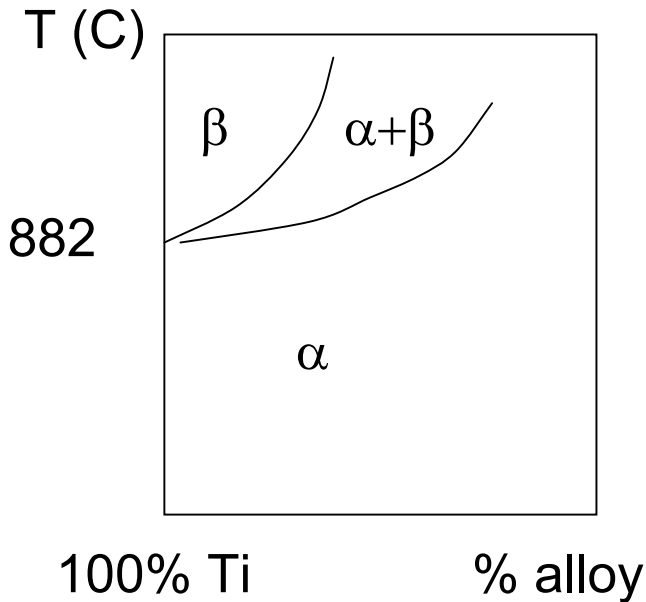
- Outstanding resistance to corrosion in oxidising chloride environments
- High melting temperature (1667 C) therefore good creep resistance
- Susceptible to catching fire – limited to temperatures of 400 C in aero engines
- Density 4.5 Mg m^{-3}
- HCP (α) at low T – transforms to BCC (β) at 882 °C

Alloying Elements

α phase
stabilisers
Al O C N

β phase
isomorphous
stabilisers
Mo, V, Nb, Ta

β phase
eutectic
stabilisers
Fe Cr Mn



Alloys

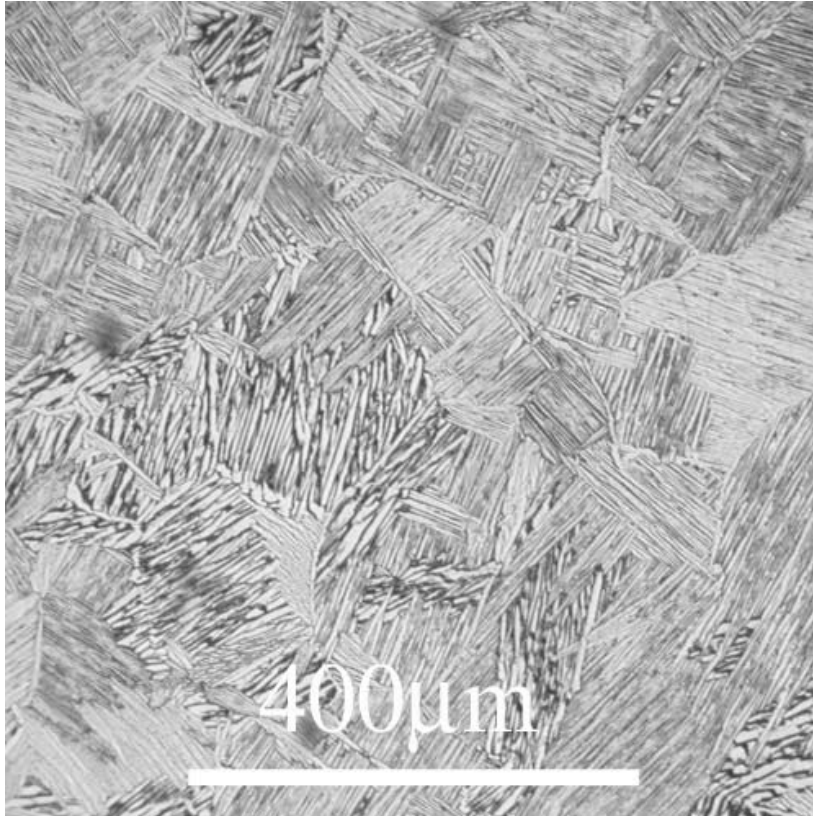
- Near α alloys
 - Al main alloying element
 - Zr, Sn added for solution strengthening
 - Mo added to give some β phase (ductility)
- $\alpha + \beta$ alloys - Ti 6%Al 4%V
 - Al provides strength and reduces weight. V increases β phase giving good ductility
 - 50% all Ti produced
 - Good strength (1100 MPa), creep resistance and fatigue resistance
 - Ductile to brittle transition (bcc). Brittle fracture at room T
 - Heat treatable – controlled transformation from β to α to improve strength

Ti alloys

- β phase – Ti 35%V 15% Cr
 - Burn resistant alloy, increases operating temperature to 510 C

- Titanium Alumides
 - Laminar structure made up from layers of hexagonal Ti_3Al and tetragonal $TiAl$
 - High strength, low density, good creep resistance
 - Used extensively for aerospace turbochargers

Ti - Microstructure



The α hcp phase (light) precipitates out as plates from the high T β bcc phase (dark)

Ti 6% Al 4% V

Ti - uses

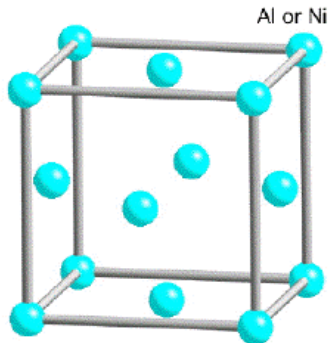
- Jet engines
- Ships propellers
- Chemical plants
- Artificial hips
- Sports equipment
 - Golf clubs and balls
 - Baseball bats
 - Tennis rackets
 - Bicycle frames
- Glasses frames
- Jewellery
- Architecture (Guggenheim museum in Bilbao)

Ni Based Superalloys

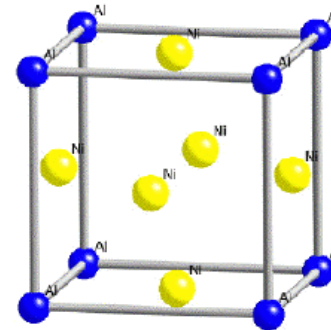
- A superalloy is one that can be used at high T
– up to $0.7 T_m$
- Creep and oxidation resistance are the main design criteria
- Superalloys are based on Fe, Co or Ni
- Ni generally must suitable for aero engine applications

Alloys

- Alloying metal is either Al or Ti
- 2 phases – very similar lattice parameters



γ – solid solution with fcc structure

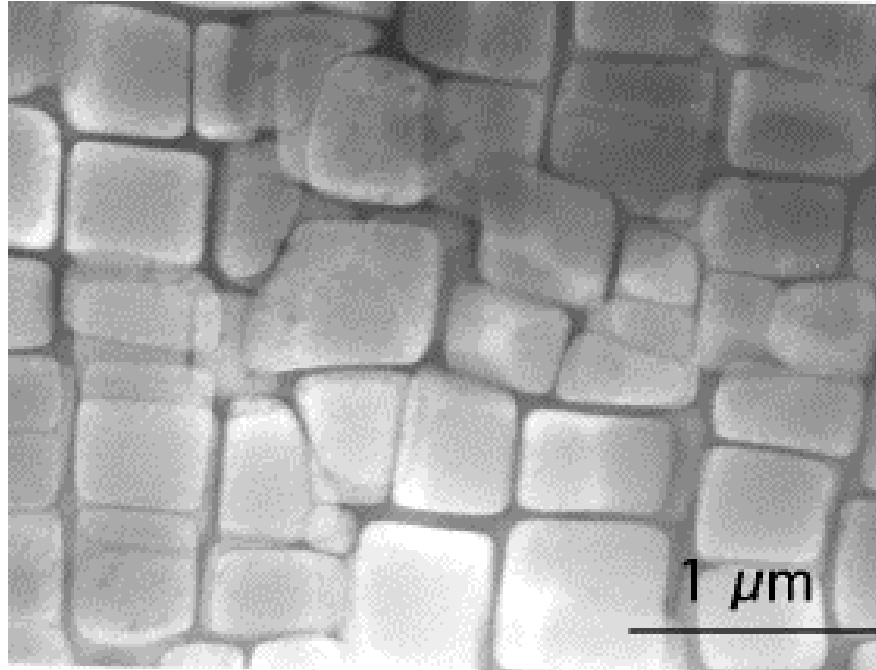


γ' – intermetallic compound Ni_3Al with cubic structure. Al on cube edges and Ni in face centres

Properties

- Small lattice misfit between phases leads to small interfacial energy
 - Coarsening driven by interfacial energy
 - Small precipitates stable
- Dislocations find it difficult to move from γ into γ' because this would disrupt local ordering
- Strength independent of temperature up to 600 C because dislocations trapped on γ' phase

Microstructure



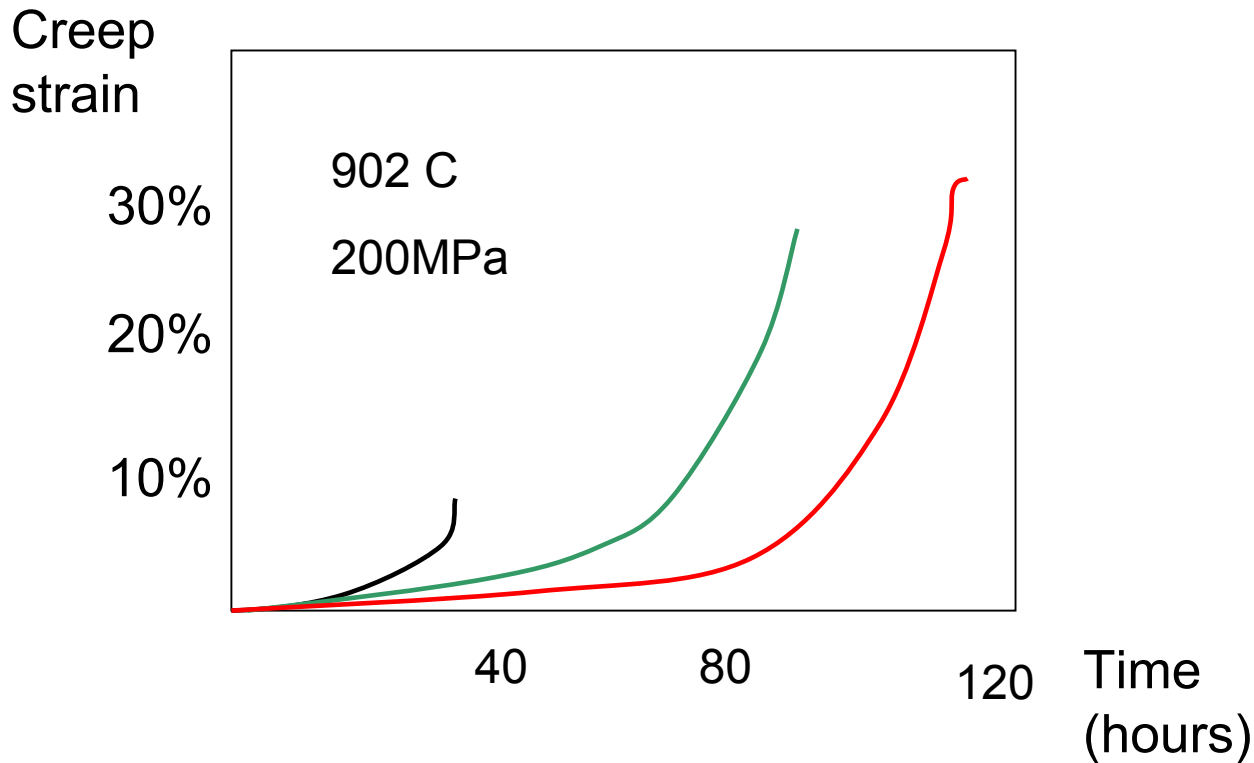
Transmission electron micrograph showing a large fraction of cuboidal γ' particles in a γ matrix. Ni-9.7Al-1.7Ti-17.1Cr-6.3Co-2.3W at%. Hillier, Ph.D. Thesis, University of Cambridge, 1984.

Alloys

- Al (up to 10%) to add γ' phase
- Ti – goes into γ' to give solid solution strengthening
- Cr – goes into γ (Ni) phase to give corrosion resistance and solid solution strengthening
- Co – goes into both γ and γ' – enhances γ' formation

Creep Resistance

- Creep resistance improved by
 - Directional solidification
 - Single crystal solidification



What makes metals suitable base for alloys?

- Readily available and cheap
- High melting T
- Cubic crystal structure
- Low density
- Readily dissolves solutes
- Solubility varies strongly with temperature
- Forms hard compounds
- Undergoes an allotropic phase change
- Chemically stable
- Not hazardous