

# 1.033/1.57 H#2: Stress & Strength

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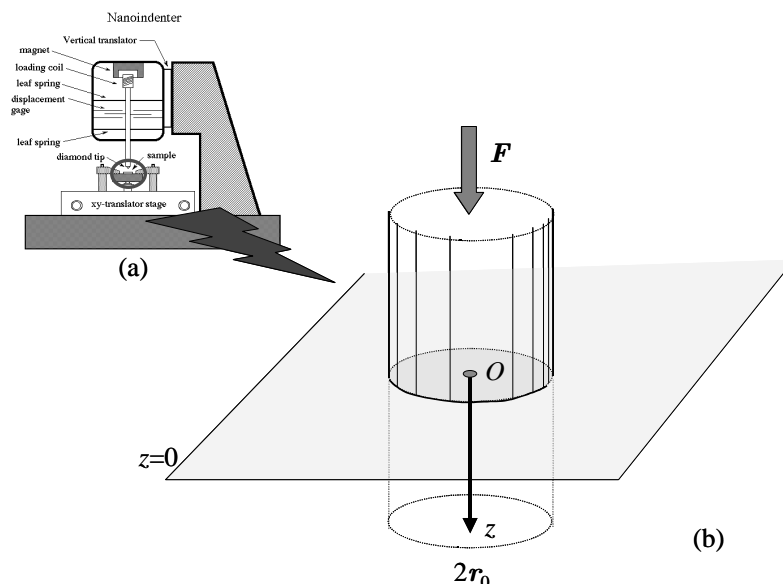
**Instrumented Nano-Indentation:** Instrumented nano-indentation is a new technique in materials science and engineering to determine material strengths at very fine scales. The test consists in a penetration of a needle-type indenter in a continuous material system (see experimental setup in figure (a) below). The force required to penetrate is then related to the strength of the material – by means of mechanical modeling.

In this exercise, we propose to develop a simplified triaxial stress–strength model of the nano-indentation test. To simplify the problem, we consider that the indenter is a rigid cylinder of radius  $r_0$ , situated on the surface of a horizontal half-space composed of a homogeneous material, as sketched in figure (b) below. A vertical force  $F$  is exerted on the cylinder in the direction of the cylinder axis  $Oz$ , until it penetrates into the half-space. The value of the force  $F$  at this moment is noted  $\max F$ , and the material property that is reported from the test is known as micro-hardness:

$$H = \frac{\max F}{A}$$

where  $A$  is the contact area of the indenter with the material. We suppose that the contact of the cylinder with the half-space (at  $z = 0; r \leq r_0$ ) is without friction. Aim of this exercise is to relate the micro-hardness measurement to the strength properties of the material composing the half-space.

Throughout this exercise we will assume quasi-static conditions (inertia effects neglected), and we will neglect body forces.



Nano-Indentation test: (a) Experimental Setup; (b) Simplified Mechanical Model.

1. **Statically Admissible Stress Field:** For purpose of analysis, we separate the half-space  $\Omega$  in two subdomains, noted respectively  $\Omega_1$  and  $\Omega_2$ . In these domains, we consider the following stress fields:

- in  $\Omega_1$  defined by  $z > 0$  and  $r < r_0$ :

$$\sigma'_{rr} = q'; \quad \sigma'_{\theta\theta} = q''; \quad \sigma'_{zz} = \sigma \quad (\text{other } \sigma'_{ij} = 0)$$

- in  $\Omega_2$  defined by  $z > 0$  and  $r > r_0$ :

$$\sigma'_{rr} = -q(r_0/r)^2; \quad \sigma'_{\theta\theta} = q(r_0/r)^2 \quad (\text{other } \sigma'_{ij} = 0)$$

- Specify precisely ALL conditions which statically admissible stress fields in  $\Omega_1$  and  $\Omega_2$  need to satisfy.
  - Determine the constants  $q'$ ,  $q''$ ,  $q$  and  $\sigma$ , so that the stress field  $\sigma'$  is statically admissible in  $\Omega = \Omega_1 \cup \Omega_2$ .
  - In the Mohr Plane ( $\sigma \times \tau$ ), give a graphical representation of the stress field  $\sigma'$  for  $\Omega_1$  and  $\Omega_2$ , by considering that  $F > q\pi r_0^2$ . In both Mohr Plane and material plane, determine the surface and the corresponding stress vector, where the shear stress is maximum in  $\Omega$ .
2. **Mohr-Coulomb Strength Criterion:** The material we consider is a Mohr-Coulomb material, for which the strength domain is defined by:

$$f(\boldsymbol{\sigma}) = |\tau| + \sigma \tan \varphi - c \leq 0$$

where  $|\tau| = \sqrt{\mathbf{T}^2 - \sigma^2}$ ,  $\sigma = \mathbf{n} \cdot \boldsymbol{\sigma} \cdot \mathbf{n}$ ;  $\tan \varphi$  is the friction coefficient, and  $c$  is the cohesion. Alternatively, the Mohr-Coulomb criterion can be written in terms of the principal stresses  $\sigma_I \geq \sigma_{II} \geq \sigma_{III}$ :

$$f(\boldsymbol{\sigma}) = \sigma_I(1 + \sin \varphi) - \sigma_{III}(1 - \sin \varphi) - 2c \cos \varphi \leq 0$$

- Display the Mohr-Coulomb criterion in the Mohr Plane ( $\sigma \times \tau$ );
  - Determine the relation between micro-hardness  $H$  and the strength material properties of the Mohr-Coulomb criterion.
  - In the material plane, represent the orientation of the critical material surfaces, on which the Mohr-Coulomb criterion is reached.
3. **Refined Approach:** By considering that the stress field in  $\Omega_2$  was constant, determine a second relation between the micro-hardness  $H$  and the Mohr-Coulomb model parameters. Which of the two solutions is closer to the 'real' maximum micro-hardness value at failure of the Mohr-Coulomb material system. Say why (HINT: Sketch your response in the Mohr-Plane)?