

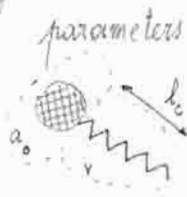
- Outline:
- finish shape factors / aggregation
  - membrane mechanics: stretch, bend, shear
  - micropipette experiments:
    - pure lipid bilayers
    - neutrophils (white blood cells)
    - red blood cells

Review of L # 19

Cell structural components: membrane, cytoskeleton, nucleus & organelles, cytosol

Geometric arguments for self-assembly:

- geometric packing with 3 parameters



$a_0$ : area occupied by head group  
 $v$ : volume of tail  
 $l_c$ : critical length\* of hydrocarbon chain  
 $l_c \ll$  contour length  
 \* over which it remains "fluid like"

$$\text{dimensionless group} = \frac{v}{a_0 l_c}$$

hence micelle



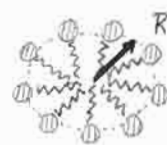
or bilayer



- example spherical micelles

Radius  $R$   
 Area  $4\pi R^2$   
 Volume  $\frac{4}{3}\pi R^3$

know  $a_0$  and  $v$  for amphiphile



$$\text{number of micelles} = \frac{4\pi R^2}{a_0} = \frac{4\pi R^3}{3v}$$

hence  $\frac{v}{a_0 R} = \frac{1}{3}$  and because  $R \ll l_c$ , we have

$$\frac{v}{a_0 l_c} \ll \frac{1}{3}$$

Amphiphiles with 2 tails are a good biological design

- low CMC
- large residence times
- spherical containers

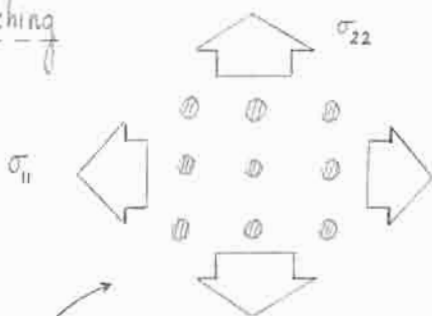


energy cost for binding / closing  
 $\ll$   
 hydrophobic energy at ends

Membrane mechanics

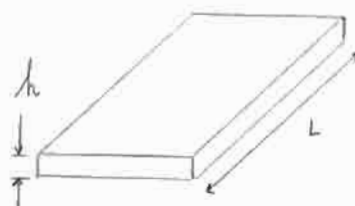
Major modes of deformation: stretch / bend / shear

Stretching

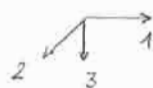


top view, stretching exposes hydrophobic core  $\Rightarrow$  resists

Model of a thin plate:



$h \ll L$   
 5 nm microns



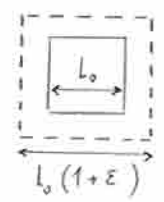
- homogeneous ideal elastic HIE hypothesis

$$\epsilon_{11} = \frac{1-\nu}{E} \sigma_{11} - \frac{\nu}{E} (\sigma_{11} + \sigma_{22} + \sigma_{33}) \quad \text{and for } \epsilon_{11} = \epsilon_{22} = \epsilon, \sigma_{11} = \sigma_{22} = \sigma$$

$$\sigma = \frac{E}{1-\nu} \epsilon$$

- expansion of area

$$\frac{\Delta A}{A_0} = \frac{(L_0 + \epsilon L_0)^2 - L_0^2}{L_0^2} \approx 2\epsilon$$



$$\sigma = \frac{E}{2(1-\nu)} \frac{\Delta A}{A_0}$$

- define a surface tension N

$$[N] = [\text{Force} / \text{Length}]$$

$$[\sigma] = [\text{Force} / \text{Length}^2]$$

$N_1 = \int_{-h/2}^{h/2} \sigma_{11} dx_3$  : integrate over width of plate, so here  $\sigma h = N$

$$N = \frac{Eh}{2(1-\nu)} \frac{\Delta A}{A_0} = K_e \frac{\Delta A}{A_0}$$

with area expansion modulus for HIE

$$K_e = \frac{Eh}{2(1-\nu)}$$

- Typical numbers for  $K_e$  :

pure lipid bilayer	~ 0.1 - 0.2	N/m
red blood cell (cortex)	~ 0.45	N/m (Evans & Wayte)
water / air interface	~ 0.07	N/m

rupture for modest strains :  $\frac{\Delta A}{A_0} \sim 2-4\%$

• Pure bending



by definition  $M = -K_B \frac{\partial^2 u_3}{\partial x_1^2}$

M moment  
 $K_B$  bending modulus  
 curvature  $\sim \frac{1}{R}$

$$K_B = \frac{Eh^3}{12(1-\nu^2)}$$

bending modulus for HIE

- Typical values of  $K_B$  (energy)

pure lipid bilayer	~ 10 - 30	kT
red blood cell	~ 10 - 30	kT

• Shear : top view



- define membrane shear modulus  $\sigma_{21} = 2G \epsilon_{21}$

shear tension :  $N_{21} = 2h G \epsilon_{21}$  by integrating over the thickness

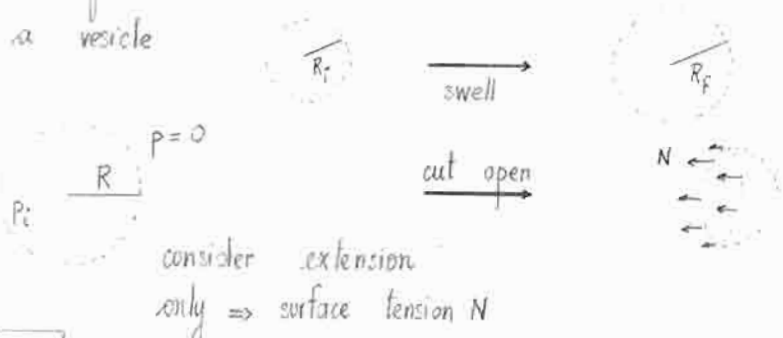
$$K_S = 2h G$$

membrane shear modulus

- experiments very easy to shear pure lipid bilayers  $\kappa_s \ll 1$  20-3  
 red blood cell  $\sim 2.5 \mu\text{N}/\text{m}$  (Hérimon 1999)

if HIE  $G = \frac{E}{2(1-\nu)}$   $\Rightarrow \left\{ \begin{array}{l} G \approx E \\ \text{shear modulus \& Young's modulus} \end{array} \right.$  have the same order of magnitude  
 because  $\left. \begin{array}{l} \kappa_s \approx h G \\ \kappa_e \approx h E \end{array} \right\}$  would expect  $\kappa_s \approx \kappa_e$ , but very far off!  
 HIE not perfect

• Osmotic swelling  
 - create a vesicle



Radius by light scattering

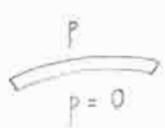
$$2\pi R N = p_i \pi R^2$$

(projection onto cut plane)  
 surface tension = pressure

$$p_i = \frac{2N}{R}$$

Laplace's equation

• Scaling analysis of bending & tension (details in Roger Kamm's manuscript: Ch. 2.1 p.13)



$$p + N \underbrace{\frac{\partial^2 u_3}{\partial x_1^2}}_{\text{curvature}} - \underbrace{\kappa_B \frac{\partial^4 u_3}{\partial x_1^4}}_{\text{bending}} = 0$$

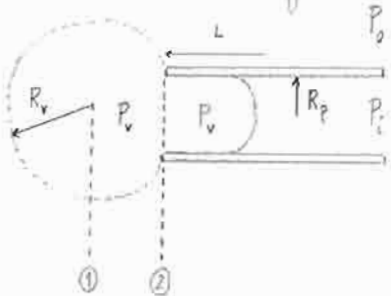
- order of magnitude of these two effects:  
 - bending  $\kappa_B \frac{\partial^4 u_3}{\partial x_1^4} \sim \kappa_B \frac{u_3}{L^4}$   
 - tension  $N \frac{\partial^2 u_3}{\partial x_1^2} \sim N \frac{u_3}{L^2}$

$L \equiv$  characteristic dimension over which  $u_3$  varies

$$\frac{\text{bending}}{\text{tension}} \sim \frac{\kappa_B}{NL^2}$$

$\left\{ \begin{array}{l} \text{if } \ll 1 \\ \text{if } \gg 1 \end{array} \right.$  get rid of bending term in balance equation  
 " " " "

□ Micropipette aspiration only consider N



- force balance

$$\left. \begin{array}{l} \textcircled{1} p_v - p_o = \frac{2N}{R_v} \\ \textcircled{2} p_v - p_i = \frac{2N}{R_p} \end{array} \right\}$$

$$N = \frac{1}{2} (p_o - p_i) \left( \frac{1}{R_p} - \frac{1}{R_v} \right)^{-1}$$

- get  $\frac{\Delta A}{A_0}$  from geometric arguments

$$\frac{\Delta A}{A_0} = \frac{R_p^2}{2R_v^2} \left( \frac{1}{R_p} - \frac{1}{R_v} \right) L$$

lipid bilayer: N  $\nearrow$  with strain  
 neutrophil: constant N  
 ruffled membrane