Monochromatic Radiation is Always 100% Polarized



Polarization Ellipse



e.g. a, b, φ Also, (need "+" or "-" a, φ , θ to \Rightarrow right or left elliptical) v_x , v_y , θ

Polarization of Narrowband Radiation

Let $\overline{E}(t) = \hat{x}v_{x}(t)\cos[\omega t + \phi(t)] + \hat{y}v_{y}(t)\cos[\omega t + \phi(t) + \delta(t)]$

 $v_x(t)$ and $v_y(t)$ are slowly varying and random; $\langle v_x \rangle$, $\langle v_y \rangle$, and $\langle \delta \rangle$ may be non-zero

"Stokes Parameters"

 $I \equiv S_{o} \equiv \frac{\left| \left\langle v_{x}^{2}(t) \right\rangle + \left\langle v_{y}^{2}(t) \right\rangle \right|}{2n_{o}}$ [W m⁻²] total power $Q \equiv S_{0} \equiv \frac{\left[\left\langle v_{x}^{2}(t)\right\rangle - \left\langle v_{y}^{2}(t)\right\rangle\right]}{2\eta_{0}}$ "x-ness" $U \equiv S_2 \equiv \frac{2 \left\langle v_x(t) \bullet v_y(t) \cos \delta(t) \right\rangle}{2 \eta_0}$ "45°-ness" $V \equiv S_3 \equiv \frac{2 \langle v_x(t) \bullet v_y(t) \sin \delta(t) \rangle}{2 \eta_0}$ "circularity"

100% Polarized Narrowband Waves

Let $\overline{E}(t) = \hat{x}v_{x}(t)\cos[\omega t + \phi(t)] + \hat{y}v_{y}(t)\cos[\omega t + \phi(t) + \delta(t)]$

 $v_x(t)$ and $v_y(t)$ are slowly varying and random; $\langle v_x \rangle$, $\langle v_y \rangle$, and $\langle \delta \rangle$ may be non-zero

 $\delta(t) = \delta_0$ and $v_x/v_y(t) = constant \Rightarrow fixed ellipse, variable size$



Also:
$$S_0^2 = S_1^2 + S_2^2 + S_3^2$$

Therefore, any 3 Stokes parameters specify polarization

Partially Polarized Narrowband Radiation

"Stokes Parameters"

$$I \equiv S_{o} \equiv \frac{\left[\langle v_{x}^{2}(t) \rangle + \langle v_{y}^{2}(t) \rangle\right]}{2\eta_{o}}$$
$$Q \equiv S_{1} \equiv \frac{\left[\langle v_{x}^{2}(t) \rangle - \langle v_{y}^{2}(t) \rangle\right]}{2\eta_{o}}$$
$$U \equiv S_{o} \equiv \frac{2\langle v_{x}(t) \bullet v_{y}(t) \cos \delta(t) \rangle}{2\eta_{o}}$$

[W m⁻²] total power

"x-ness"

"45°-ness"

$$V \equiv S_3 \equiv \frac{2\langle v_x(t) \bullet v_y(t) \sin \delta(t) \rangle}{2\eta_0}$$

 $2\eta_o$

"circularity"

 $[S_0, S_1, S_2, S_3] = [S_u, 0, 0, 0] + [S_0 - S_u, S_1, S_2, S_3]$

Note: For 2 uncorrelated waves superimposed (A+B), we have $S_{i_{A+B}} = S_{i_A} + S_{i_B}$ where i = 0, 1, 2, 3

where $(S_0 - S_1)^2 = S_1^2 + S_2^2 + S_3^2$

For 0% polarization, Stokes: S_0 ; $S_1 = S_2 = S_3 = 0$

Therefore, for partially polarized wave:

Define percentage polarization = $\left(\frac{S_o - S_u}{S_o}\right) \cdot 100\%$ $\Delta = m, 0 \le m \le 1$

Lec13a.3-4 1/12/01

Coherency Matrix J

$$\underline{J} \stackrel{\Delta}{=} \frac{1}{\eta_{o}} \begin{bmatrix} \left\langle \underline{E}_{x} \underline{E}_{x}^{*} \right\rangle & \left\langle \underline{E}_{x} \underline{E}_{y}^{*} \right\rangle \\ \left\langle \underline{E}_{x}^{*} \underline{E}_{y} \right\rangle & \left\langle \underline{E}_{y} \underline{E}_{y}^{*} \right\rangle \end{bmatrix} \text{ where } E(t) = xR_{e} \left\{ \underline{E}_{x}(t)e^{j\omega t} \right\} + yR_{e} \left\{ \underline{E}_{y}(t)e^{j\omega t} \right\} \\ \text{ where } E_{x}(t), E_{y}(t) \text{ vary slowly}$$

e.g. X-polarization

$$\overline{\underline{J}}_{X} = 2S_{0} \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix}$$

RCP (right-circular)

 $\overline{\underline{J}}_{RC} = S_0 \begin{bmatrix} 1 & -j \\ j & 1 \end{bmatrix}$ $\overline{\underline{J}}_{u} = S_0 \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix}$

Unpolarized

Finding Orthogonal Polarization \overline{J}_{RC} e.g. X-polarization $\overline{J}_{X} = 2S_{0} \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix}$

RCP (right-circular)

Unpolarized

$$\underline{J}_{X} = 2S_{0} \begin{bmatrix} 0 & 0 \end{bmatrix}$$
$$\underline{J}_{RC} = S_{0} \begin{bmatrix} 1 & -j \\ j & 1 \end{bmatrix}$$
$$\underline{J}_{U} = S_{0} \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix}$$

Note: $\underline{J}_{X} + \underline{J}_{y} = 2\underline{J}_{u}$ $\underline{J}_{RC} + \underline{J}_{LC} = 2\underline{J}_{u}$ If $\frac{\underline{J}_{A} \perp \underline{J}_{B}, \text{and}}{T_{r} \underline{J}_{A} = T_{r} \overline{J}_{B}}$ then $\underline{J}_{A} + \underline{J}_{B} = 2\underline{J}_{u}$

Therefore, we can find orthogonal polarization $\overline{J}_B = 2\overline{J}_n - \overline{J}_A$

Polarized Antennas

Define
$$\frac{G_{ij}(\theta, \phi)}{G(\theta, \phi)} = \frac{A_{ij}(\theta, \phi)}{A(\theta, \phi)} = \frac{\Xi_i \Xi_j}{\Xi_x \Xi_x^* + \Xi_y \Xi_y^*}$$

e.g. $\{i, j\} = \{x, y\}, \{r, \ell\}, \{a, b\} (b \perp a)$

$$\overline{\underline{A}} = \begin{bmatrix} \underline{A}_{xx} & \underline{A}_{xy} \\ \underline{A}_{yx} & \underline{A}_{yy} \end{bmatrix}; \text{ claim } P_{rec} = \frac{1}{2} T_r \begin{bmatrix} \overline{\underline{A}} \bullet \overline{\underline{J}}_{inc} \\ \uparrow & \uparrow \end{bmatrix} [W] \text{ for incident plane wave } precession precession precession of the set of the set$$

Polarized Antennas

$$\overline{\underline{A}} = \begin{bmatrix} \underline{A}_{xx} & \underline{A}_{xy} \\ \underline{A}_{yx} & \underline{A}_{yy} \end{bmatrix}; \text{ claim } P_{\text{rec}} = \frac{1}{2} T_{r} \begin{bmatrix} \overline{\underline{A}} \bullet \overline{\underline{J}}_{\text{inc}}^{t} \end{bmatrix} \begin{bmatrix} W \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yx} & \underline{A}_{yy} \end{bmatrix}; \text{ claim } P_{\text{rec}} = \frac{1}{2} T_{r} \begin{bmatrix} \overline{\underline{A}} \bullet \overline{\underline{J}}_{\text{inc}}^{t} \end{bmatrix} \begin{bmatrix} W \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yx} & \underline{A}_{yy} \end{bmatrix}; \text{ claim } P_{\text{rec}} = \frac{1}{2} T_{r} \begin{bmatrix} \overline{\underline{A}} \bullet \overline{\underline{J}}_{\text{inc}}^{t} \end{bmatrix} \begin{bmatrix} W \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yx} & \underline{A}_{yy} \end{bmatrix}; \text{ claim } P_{\text{rec}} = \frac{1}{2} T_{r} \begin{bmatrix} \overline{\underline{A}} \bullet \overline{\underline{J}}_{\text{inc}} \end{bmatrix} \begin{bmatrix} W \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident plane wave } \begin{bmatrix} \underline{A}_{yy} & \underline{A}_{yy} \end{bmatrix} \text{ for incident pl$$

So
$$P_{rec} = \frac{1}{2} [A_{11}J_{11} + A_{12}J_{12} + A_{21}J_{21} + A_{22}J_{22}]$$

for incident uniform plane wave \overline{J} on antenna \overline{A}

For
$$\Omega_{s} \neq 0$$
: $P_{rec} = \frac{1}{2} \int_{4\pi} T_{r} \left[\overline{\underline{A}}(\theta, \phi) \overline{\underline{J}}^{t}(\theta, \phi) \right] d\Omega$

To Measure Polarization

Measure 4 powers; use 4 antennas

e.g.
$$\begin{bmatrix} M_{a} \\ M_{b} \\ M_{c} \\ M_{d} \end{bmatrix} = \frac{1}{2} \begin{bmatrix} \underline{A}_{11_{a}} & \underline{A}_{12_{a}} & \underline{A}_{21_{a}} & \underline{A}_{22_{a}} \\ \underline{A}_{11_{b}} & \underline{A}_{12_{b}} & \bullet & \bullet \\ \underline{A}_{11_{c}} & \bullet & \bullet & \bullet \\ \underline{A}_{11_{c}} & \bullet & \bullet & \underline{A}_{11_{d}} \end{bmatrix} \begin{bmatrix} \underline{J}_{11} \\ \underline{J}_{12} \\ \underline{J}_{21} \\ \underline{J}_{22} \end{bmatrix}$$

$$\overline{M} = \frac{1}{2}\overline{\underline{A}}\overline{\underline{J}}, \text{ so } \overline{\underline{J}} = 2\overline{\underline{A}}^{-1}\overline{M}\left(\overline{\underline{J}} \text{ is estimate}\right)$$

Is $\overline{\underline{A}}$ singular?

To Measure Polarization $\overline{M} = \frac{1}{2}\overline{\overline{A}}\overline{\overline{J}}$, so $\overline{\overline{J}} = 2\overline{\overline{A}}^{-1}\overline{M}(\overline{\overline{J}}$ is estimate) Is \overline{A} singular? For x, y, RC, LC POL: For x, 45°, RC, LC: $\overline{\overline{A}} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 1 & 1 & 1 & 1 \\ 1 & -j & j & 1 \\ 1 & j & -j & 1 \end{bmatrix}$ $\overline{\underline{A}} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 1 & -j & j & 1 \\ 1 & j & -j & 1 \end{bmatrix}$ Can not distinguish det $\overline{\underline{A}} = 0$ det $\overline{A} \neq 0$ "ok" vs

Example of a Polarimeter



Antenna Phase Errors



Systematic antenna phase errors:

- 1) poor design and fabrication
- 2) gravity, wind, thermal (gravity and thermal limits near 1 arc minute)
- 3) feed offset

Random antenna phase errors:

- 1) machine tolerances, surface roughness
- 2) adjustment errors
- 3) feed offset

Examples of Antenna Phase Errors

Random antenna phase errors:

- 1) matching tolerances, surface roughness
- 2) adjustment errors
- 3) feed offset

300-ft parabolic reflector antenna at NRAO, Greenbank, West Virginia

- 1) systematic sag \Rightarrow fix backup; footprints on mesh
- 2) steamrolled mesh \Rightarrow long waves
- 3) new panels: $\theta_B \ge 0.5 1$ arc minute

Types of optical and radio propagation phase errors



Effect of Phase Variation on Directivity



Effect of Phase Variation on Directivity

$$D(f,\theta,\phi) = \left[\pi (1 + \cos\theta)^2 / \lambda^2 \right] \bullet \frac{\int_A \mathbb{E}_x \left(\overline{\tau} \right) e^{-j\frac{2\pi}{\lambda} \left(\overline{\phi} \bullet \overline{\tau} \right)} d\tau_x d\tau_y}{\int_A \left| \mathbb{E}_x (x,y) \right|^2 dx dy}$$

$$E\{D(f,\theta,\phi)\} = \frac{\pi(1+\cos\theta)^2}{\lambda^2 \int_A |\underline{E}_X(x,y)|^2 dx dy} \bullet \int_A E\{\underbrace{R_{\underline{E}_X}(\bar{\tau})}_{A} e^{-j\frac{2\pi}{\lambda}(\bar{\phi}\bullet\bar{\tau})} d\tau_X d\tau_y \\ \underbrace{\int_A \underbrace{E}_X(\bar{r}) \underbrace{E}_X^*(\bar{r}-\bar{\tau}) d\bar{r}}_{E_o(\bar{r})} e^{j\gamma(\bar{r})}$$

Therefore
$$E\{R_{\underline{E}_{X}}(\bar{\tau})\} = R_{\underline{E}_{O}}(\bar{\tau})E\{e^{j\gamma(\bar{r})-j\gamma(\bar{r}-\bar{\tau})}\}$$

Spatial stationarity : $E\{e^{j\gamma(\bar{r})-j\gamma(\bar{r}-\bar{\tau})}\} = E\{e^{j\gamma(O)-j\gamma(\bar{r})}\}$

Lec13a.3-16 1/12/01

Definition of "Characteristic Function"

It is the Fourier transform of probability distribution p(x) (also called the moment-generating function)

$$\mathsf{E}\left[e^{j\omega x}\right] \equiv \int_{-\infty}^{\infty} p(x)e^{j\omega x} dx = \mathsf{F}.\mathsf{T}.[p(x)]$$

 $\stackrel{\Delta}{=} \Gamma(\omega; \mathbf{x}) = \text{``characteristic function of } \mathbf{p}(\mathbf{x})\text{''}$

One use of the Fourier transform of p(x) is when we seek $p(x_1 + x_2 + ... + x_n) =$

$$p(x_1) * p(x_2) * ... * p(x_n) = F.T. \begin{cases} n \\ \pi \\ i=1 \end{cases} F.T. [p(x_i)] \end{cases}$$

Computation of $E\{R_{E_x}(\bar{\tau})\}$

Thus $\Gamma(\omega_1, \omega_2; \gamma(0), \gamma(\overline{\tau})) = \mathsf{E}\left\{ e^{j\omega_1\gamma(0) + j\omega_2\gamma(\overline{\tau})} \right\}$

Recall: If $\underline{\gamma}_1, \underline{\gamma}_2$ are JGRV, then $\Gamma(\omega_1, \omega_2, \underline{\gamma}_1, \underline{\gamma}_2) = e^{-\frac{1}{2}[\omega_1 \omega_2]} \begin{bmatrix} \underline{\gamma}_1 \underline{\gamma}_1^* & \underline{\gamma}_1 \underline{\gamma}_2^* \\ \underline{\gamma}_2 \underline{\gamma}_1^* & \underline{\gamma}_2 \underline{\gamma}_2^* \end{bmatrix} \begin{bmatrix} \omega_1 \\ \omega_2 \end{bmatrix}$

Here, $\gamma_1 \stackrel{\Delta}{=} \gamma(0)$, $\gamma_2 \stackrel{\Delta}{=} \gamma(\overline{\tau})$

Therefore: $\mathsf{E}\left\{\mathsf{e}^{j\gamma(0)-j\gamma(\tau)}\right\} = \Gamma\left(\omega_1 = 1, \omega_2 = -1; \gamma(0), \gamma(\tau)\right)$

Computation of $E\{R_{E_{\tau}}(\bar{\tau})\}$ $\Gamma(\omega_{1},\omega_{2},\underline{\gamma}_{1},\underline{\gamma}_{2}) = e^{-\frac{1}{2}[\omega_{1}\omega_{2}]} \begin{bmatrix} \underline{\gamma}_{1}\underline{\gamma}_{1}^{*} & \underline{\gamma}_{1}\underline{\gamma}_{2}^{*} \\ \underline{\gamma}_{2}\underline{\gamma}_{1}^{*} & \underline{\gamma}_{2}\underline{\gamma}_{2}^{*} \end{bmatrix}} \begin{bmatrix} \omega_{1} \\ \omega_{2} \end{bmatrix}$ Here, $\gamma_{1} \stackrel{\Delta}{=} \gamma(0)$, $\gamma_{2} \stackrel{\Delta}{=} \gamma(\overline{\tau})$ Therefore: $\mathsf{E}\left\{\mathsf{e}^{j\gamma(0)}, \gamma(\overline{\tau})\right\} = \Gamma\left(\omega_1 = 1, \omega_2 = -1; \gamma(0), \gamma(\overline{\tau})\right)$ Since: $\underline{\gamma}(0)\underline{\gamma}^{*}(0) \stackrel{\Delta}{=} \phi(0)$ $\underline{\gamma}(0)\underline{\gamma}^{*}(\overline{\tau}) \stackrel{\Delta}{=} \phi(\overline{\tau})$ $\underline{\gamma}(\overline{\tau})\underline{\gamma}^{*}(\overline{\tau}) = \phi(0) \leftarrow \text{by stationarity}$ $\left(\omega_{1}=1, \omega_{2}=-1; \gamma(0), \gamma(\overline{\tau})\right)=e^{-\frac{1}{2}\left[1-1\right]}\begin{bmatrix}\phi(0) & \phi(\tau)\\ \phi^{*}(\tau) & \phi(0)\end{bmatrix}\begin{bmatrix}1\\-1\end{bmatrix}$ $= \mathbf{e}^{\phi(\tau)} - \phi(0)$ Therefore $E\{R_{\underline{E}_{X}}(\bar{\tau})\} = R_{E_{O}}(\bar{\tau}) \bullet e^{\phi(\bar{\tau})} - \phi(0)$

1/12/0′

Computation of Expected Directivity

$$\mathsf{E}\left\{\mathsf{D}(\mathsf{f},\theta,\phi)\right\} = \left[\frac{\pi(\mathsf{1}+\cos\theta)^{2}}{\lambda^{2}\int_{A}\left|\left|\mathsf{E}\left(\bar{r}\right)\right|^{2}\mathsf{d}a}\right] \bullet \int_{A}\left[e^{\phi\left(\bar{\tau}\right)-\phi\left(0\right)} \mathsf{R}_{E_{0}}\left(\bar{\tau}\right)\right]e^{-j\frac{2\pi-\bar{\tau}}{\lambda}} \, d\tau_{x}d\tau_{y}$$









Solution to Expected Directivity





Lec13a.3-21 1/12/01

Examples of Random Antenna Surface Let b = RMS surface tolerance of reflector antenna On-axis gain of random antenna $|G'_{0} = G_{0}e^{-\sigma^{2}} = G_{0}e^{-(2b \bullet 2\pi/\lambda)^{2}} = G_{0}e^{-(b4\pi/\lambda)^{2}}$ If b = $\lambda/4\pi \implies G_0 \bullet e^{-1}$ $b = \lambda/16 \implies G_0 \bullet 0.54$ new $b = \lambda/32 \implies G_0 \bullet 0.9$ [↑]log G (power shifts to sidelobes) Any aperture antenna, fixed $\log G = -2\log \lambda + \log 4\pi A_{P}$ illumination -2 → log λ ~minimum useful wavelength Lec13a.3-22 X11 1/12/01